



A new mixed finite
element
formulation for
reorientation in
liquid crystalline
elastomers

Groß M., Dietzsch
J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based
weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Professorship of Applied Mechanics and Dynamics

Faculty of Mechanical Engineering

JoyMech 2022 (in-person event) 24–26 August

Acknowledgment: This lecture is dedicated to Professor Paul Steinmann
and provided by **DFG** under the grant GR 3297/7-1

Motivation and goals

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

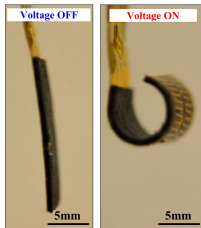
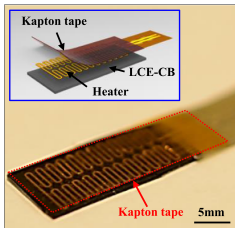
Initial rotation

Temperature control

Transient heat flux load

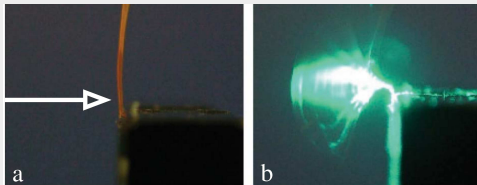
Summary

Goal 1: FE simulation of thermal actuation of motion of a LCE material



Introducing **Joule heat** power by heating pads, see Cui Y. et al. [2018]

Goal 2: FE simulation of UV light acuation of motion of a LCE material



Using **UV light** for inducing vibrations, see Corbett & Warner [2009]

Step 1: FE formulation for actuation of continuum motions by boundary or volume loads

We design a **dynamic mixed FE method** for continuum motions with **internal reorientation**

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

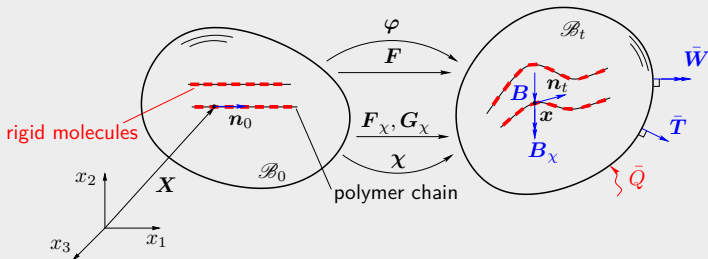
Initial rotation

Temperature control

Transient heat flux load

Summary

Continuum configurations of a LCE with boundary/volume loads



1 Orientation mapping

$$\chi: \mathcal{B}_0 \times \mathcal{T} \rightarrow \mathbb{R}^{n_{\text{dim}}} \text{ with}$$

$$\chi(\mathbf{X}, 0) = \mathbf{n}_0(\mathbf{X}) \text{ and } \mathbf{n}_0 \cdot \mathbf{n}_0 = 1$$

2 Orientation tensor

$$\mathbf{F}_\chi := \chi \otimes \mathbf{n}_0 \quad \mathbf{n}_t = \mathbf{F}_\chi \mathbf{n}_0$$

3 Orient. deformation tensor

$$\mathbf{C}_\chi := \mathbf{F}^t \mathbf{g} \mathbf{F}_\chi = \mathbf{F}^t \mathbf{g}_\chi \mathbf{F}$$

4 Distorsion tensor

$$\mathbf{K}_\chi := \mathbf{F}^t \mathbf{g} \mathbf{G}_\chi = \mathbf{F}^t \mathbf{g}_K \mathbf{F}$$

5 Orient. velocity vector

$$\mathbf{v}_\chi(\mathbf{X}, t) := \dot{\chi}(\mathbf{X}, t) = \dot{\mathbf{n}}_t$$

6 Orient. momentum vector

$$\mathbf{p}_\chi := \rho_0 \left[(l_\chi^2 - l_0^2) \mathbf{A}_0 + l_0^2 \mathbf{I} \right] \mathbf{v}_\chi$$

$$\mathbf{A}_0 := \mathbf{n}_0 \otimes \mathbf{n}_0$$

Free energy functions as stress potentials

(cp. Frank [1958], Leslie [1968], Warner et al. [1993], Anderson et al. [1999], Himpel et al. [2008], De Luca et al. [2013])

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

Free energy of thermo-orientational deformations

- Interactive free energy

$$\Psi_i(\mathbf{F}^t \mathbf{g} \boldsymbol{\chi}, \Theta) \equiv \Psi^{\text{ori}}(\mathbf{C}_\chi, \Theta) := \hat{\Psi}^{\text{ori}}(I_1^{\text{ori}}, J_2^{\text{ori}}, \Theta)$$

- Oriental invariants

$$I_1^{\text{ori}} := \mathbf{C}_\chi \mathbf{A}_0 : \mathbf{G}^{-1} \qquad J_2^{\text{ori}} := \mathbf{C}_\chi \mathbf{A}_0 : \mathbf{C}_\chi \mathbf{A}_0$$

Free energy associated with distortions of the orientation field

- Frank free energy

$$\Psi^{\text{dis}}(\mathbf{K}_\chi) := \hat{\Psi}^{\text{dis}}(I_1^{\text{dis}}, J_2^{\text{dis}})$$

- Distorsional invariants

$$I_1^{\text{dis}} := (\mathbf{K}_\chi - \text{Grad}[\mathbf{n}_0]) : \mathbf{G}^{-1} \qquad J_2^{\text{dis}} := (\mathbf{K}_\chi - \text{Grad}[\mathbf{n}_0]) : (\mathbf{K}_\chi - \text{Grad}[\mathbf{n}_0])$$

Free energy of thermo-elastic deformations

- Compressible free energy

$$\Psi^{\text{ela}}(\mathbf{C}, \Theta) := \hat{\Psi}^{\text{ela}}(I_1^{\text{ela}}, J_2^{\text{ela}}, I_3^{\text{ela}}, \Theta)$$

- Deformation invariants

$$I_1^{\text{ela}} := \mathbf{C} : \mathbf{G}^{-1} \qquad J_2^{\text{ela}} := \mathbf{C} : \mathbf{C} \qquad I_3^{\text{ela}} := \det[\mathbf{C}]$$

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

Duhamel's law for transverse isotropy with reorientation

- 1 Cauchy heat flux vector

$$\mathbf{q} := -\mathbf{k}^{\text{cdu}} \text{grad}[\Theta] \quad \mathbf{k}^{\text{cdu}} := k_n \boldsymbol{\chi} \otimes \boldsymbol{\chi} + k_0 (\mathbf{g}^{-1} - \boldsymbol{\chi} \otimes \boldsymbol{\chi})$$

- 2 Piola transformation and orientation tensor

$$\det[\mathbf{F}]^{-1} \mathbf{F} \mathbf{Q} = -\mathbf{k}^{\text{cdu}} \mathbf{F}^{-t} \text{Grad}[\Theta] \quad \boldsymbol{\chi} := \mathbf{F}_\chi \mathbf{n}_0$$

- 3 Piola heat flux vector

$$\mathbf{Q} := -\mathbf{K}^{\text{cdu}} \text{Grad}[\Theta] \quad \mathbf{K}^{\text{cdu}} := \det[\mathbf{F}] [(k_n - k_0) \mathbf{C}^{-1} \mathbf{C}_\chi \mathbf{A}_0 \mathbf{C}_\chi^t \mathbf{C}^{-t} + k_0 \mathbf{C}^{-1}]$$

Thermomech. coupling for transverse isotropy with reorientation

- 1 Coupling parameters

$$\alpha_0 (\Theta - \Theta_\infty) := \sqrt{I_3^{\text{ela}}} - 1 \quad \beta_n (\Theta - \Theta_\infty) := \sqrt{J_2^{\text{ori}}} - 1$$

- 2 Coupling free energy functions

$$\Psi_{\text{the}}^{\text{ela}}(\mathbf{C}, \Theta) := -2 \sqrt{I_3^{\text{ela}}} \alpha_0 (\Theta - \Theta_\infty) \frac{\partial \Psi_{\text{vol}}^{\text{ela}}(I_3^{\text{ela}})}{\partial I_3^{\text{ela}}}$$

$$\Psi_{\text{the}}^{\text{ori}}(\mathbf{C}_\chi, \Theta) := -2 \sqrt{J_2^{\text{ori}}} \beta_n (\Theta - \Theta_\infty) \frac{\partial \Psi_{\text{II}}^{\text{ori}}(J_2^{\text{ori}})}{\partial J_2^{\text{ori}}}$$

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

Reorientation modelled as dissipative process

(cp. Garikipati et al. [2006])

- 1 (Non-isothermal) Clausius-Planck inequality

$$D_{\chi}^{\text{int}} := \mathbf{N}_{\chi} : \mathbf{g} \dot{\mathbf{F}} - \dot{\Psi}^{\text{ori}}(\mathbf{C}_{\chi}, \Theta) - \eta_{\chi} \dot{\Theta} \geq 0$$

- 2 Normalized orientation vectors guaranteed by drilling degrees of freedom

$$\mathbb{I}^{\text{skw}} : \mathbf{g} \dot{\mathbf{F}}_{\chi} \mathbf{F}_{\chi}^{-1} = \epsilon \cdot \dot{\alpha} \quad \dot{\alpha} := \dot{\alpha}^k \mathbf{g}_k \circ \varphi(\mathbf{X}, t)$$

- 3 Reorientation dissipation

$$D_{\chi}^{\text{int}} := [\mathbf{N}_{\chi} - \mathbf{F}_{\chi} \mathbf{S}_{\chi}^t] : \mathbf{g} \dot{\mathbf{F}} - \left[\frac{\partial \Psi^{\text{ori}}(\mathbf{C}_{\chi}, \Theta)}{\partial \Theta} + \eta_{\chi} \right] \dot{\Theta} - \tau_{\chi} : \epsilon \cdot \dot{\alpha} \geq 0$$

- 4 Coleman-Noll procedure

$$\mathbf{N}_{\chi} := \mathbf{F}_{\chi} \mathbf{S}_{\chi}^t \quad \tau_{\chi} := \mathbf{F} \mathbf{S}_{\chi} \mathbf{F}_{\chi}^t \quad \eta_{\chi} := - \frac{\partial \Psi^{\text{ori}}(\mathbf{C}_{\chi}, \Theta)}{\partial \Theta}$$

Reorientation equations

- 1 Orientational nonequilibrium stress equation (solved weakly on the element)

$$\boxed{-\frac{1}{2} \epsilon : \tau_{\chi} = \Sigma_{\chi}} \quad \Sigma_{\chi} = V_{\chi} \dot{\alpha} \quad D_{\chi}^{\text{int}} := 2 \Sigma_{\chi} \cdot \dot{\alpha} \geq 0$$

- 2 Global orientation equation with Dirichlet boundary conditions in general

$$\boxed{\dot{\chi} = -\epsilon \cdot \dot{\alpha} \cdot \chi}$$

Principle of virtual power extended to mixed fields

- 1 Incremental principle of virtual power

$$\int_{t_n}^{t_{n+1}} \delta_* \dot{\mathcal{H}}(\dot{\mathbf{U}}_1, \dots, \dot{\mathbf{U}}_s, \tilde{\mathbf{V}}_1, \dots, \tilde{\mathbf{V}}_p) dt = 0$$

- 2 Total virtual power of deformation φ , temperature Θ and orientation χ

$$\delta_* \dot{\mathcal{H}} := \delta_* \mathcal{P}_\varphi + \delta_* \mathcal{P}_\Theta + \delta_* \mathcal{P}_\chi \quad \mathcal{H} := \mathcal{T} + \Pi^{\text{int}} + \Pi^{\text{ext}}$$

Virtual power associated with the motion (I)

- 1 Virtual power of motion

$$\delta_* \mathcal{P}_\varphi := \delta_* \dot{\mathcal{T}}_\varphi(\dot{\varphi}, \dot{\mathbf{v}}, \dot{\mathbf{p}}) + \delta_* \dot{\Pi}_\varphi^{\text{ext}}(\dot{\varphi}, \tilde{\mathbf{R}}) + \delta_* \dot{\Pi}_\varphi^{\text{int}}(\dot{\varphi}, \dot{\mathbf{F}}, \dot{\mathbf{C}}, \tilde{\mathbf{P}}, \tilde{\mathbf{S}})$$

- 2 Path-independent virtual kinetic power

$$\delta_* \dot{\mathcal{T}}_\varphi(\dot{\varphi}, \dot{\mathbf{v}}, \dot{\mathbf{p}}) := \int_{\mathcal{B}_0} \delta_* \dot{\mathbf{v}} \cdot [\rho_0 \mathbf{v} - \mathbf{p}] dV + \int_{\mathcal{B}_0} \delta_* \dot{\mathbf{p}} \cdot [\dot{\varphi} - \mathbf{v}] dV + \int_{\mathcal{B}_0} \delta_* \dot{\varphi} \cdot \dot{\mathbf{p}} dV$$

- 3 Path-(in)dependent virtual external power

$$\begin{aligned} \delta_* \dot{\Pi}_\varphi^{\text{ext}}(\dot{\varphi}, \tilde{\mathbf{R}}) := & - \int_{\mathcal{B}_0} \delta_* \dot{\varphi} \cdot \mathbf{B} dV & - \int_{\partial_T \mathcal{B}_0} \delta_* \dot{\varphi} \cdot \bar{\mathbf{T}} dA \\ & - \int_{\partial_\varphi \mathcal{B}_0} \delta_* \tilde{\mathbf{R}} \cdot [\dot{\varphi} - \dot{\tilde{\varphi}}] dA & - \int_{\partial_\varphi \mathcal{B}_0} \delta_* \dot{\varphi} \cdot \tilde{\mathbf{R}} dA \end{aligned}$$

Variational-based weak formulation (II)

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

Virtual power associated with the motion (II)

Path-independent virtual internal power $\delta_* \dot{I}_\varphi^{\text{int}}(\dot{\varphi}, \dot{\tilde{\mathbf{F}}}, \dot{\tilde{\mathbf{C}}}, \tilde{\mathbf{P}}, \tilde{\mathbf{S}}) := \delta_* \mathcal{P}_\varphi^{\text{int}}$

$$\begin{aligned} \delta_* \mathcal{P}_\varphi^{\text{int}} := & \int_{\mathcal{B}_0} \delta_* \tilde{\mathbf{P}} : [\text{Grad}[\dot{\varphi}] - \dot{\tilde{\mathbf{F}}}] \, dV + \frac{1}{2} \int_{\mathcal{B}_0} \delta_* \tilde{\mathbf{S}} : \left[\frac{\partial}{\partial t} (\tilde{\mathbf{F}}^t \tilde{\mathbf{F}}) - \dot{\tilde{\mathbf{C}}} \right] \, dV \\ & + \int_{\mathcal{B}_0} \delta_* \dot{\tilde{\mathbf{C}}} : \left[\frac{\partial \Psi}{\partial \tilde{\mathbf{C}}} - \frac{1}{2} \tilde{\mathbf{S}} \right] \, dV + \int_{\mathcal{B}_0} \delta_* \dot{\tilde{\mathbf{F}}} : [\tilde{\mathbf{F}} \tilde{\mathbf{S}} - \tilde{\mathbf{P}}] \, dV + \int_{\mathcal{B}_0} \tilde{\mathbf{P}} : \text{Grad}[\delta_* \dot{\varphi}] \, dV \end{aligned}$$

Virtual power associated with the thermal evolution (I)

- 1 Virtual power of thermal evolution

$$\delta_* \mathcal{P}_\Theta := \delta_* \dot{I}_\Theta^{\text{ext}}(\dot{\Theta}, \tilde{\Theta}, \tilde{\lambda}, \tilde{h}) + \delta_* \dot{I}_\Theta^{\text{int}}(\dot{\Theta}, \dot{\eta}, \tilde{\Theta})$$

- 2 Path-dependent virtual external power

$$\begin{aligned} \delta_* \dot{I}_\Theta^{\text{ext}}(\dot{\Theta}, \tilde{\Theta}, \tilde{\lambda}, \tilde{h}) := & \int_{\mathcal{B}_0} \delta_* \tilde{\Theta} \frac{D^{\text{tot}}}{\Theta} \, dV + \int_{\mathcal{B}_0} \frac{1}{\Theta} \text{Grad}[\delta_* \tilde{\Theta}] \cdot \mathbf{Q} \, dV \\ & + \int_{\partial_Q \mathcal{B}_0} \delta_* \tilde{\Theta} \frac{\tilde{Q}}{\Theta} \, dA + \int_{\partial_\Theta \mathcal{B}_0} \delta_* \tilde{\Theta} \tilde{\lambda} \, dA - \int_{\partial_\Theta \mathcal{B}_0} \delta_* \tilde{\Theta} \tilde{h} \, dA \\ & + \int_{\partial_\Theta \mathcal{B}_0} \delta_* \tilde{\lambda} [\tilde{\Theta} - \Theta_\infty] \, dA - \int_{\partial_\Theta \mathcal{B}_0} \delta_* \tilde{h} [\dot{\Theta} - \dot{\tilde{\Theta}}] \, dA \end{aligned}$$

with

$$D^{\text{tot}} := -\frac{1}{\Theta} \text{Grad}[\tilde{\Theta}] \cdot \mathbf{Q} + 2 \dot{\alpha} \cdot \boldsymbol{\Sigma}_\chi$$

Variational-based weak formulation (III)

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

Virtual power associated with the thermal evolution (II)

Path-independent virtual internal power

$$\delta_* \dot{I}_{\Theta}^{\text{int}}(\dot{\Theta}, \dot{\eta}, \dot{\Theta}) := \int_{\mathcal{B}_0} \delta_* \dot{\Theta} \left(\frac{\partial \Psi}{\partial \Theta} + \eta \right) dV + \int_{\mathcal{B}_0} \delta_* \dot{\eta} (\Theta - \tilde{\Theta}) dV - \int_{\mathcal{B}_0} \delta_* \tilde{\Theta} \dot{\eta} dV$$

Virtual power associated with the reorientation (I)

- 1 Virtual power of reorientation

$$\delta_* \mathcal{P}_{\chi} := \delta_* \dot{\mathcal{T}}_{\chi}(\dot{\chi}, \dot{\mathbf{v}}_{\chi}, \dot{\mathbf{p}}_{\chi}) + \delta_* \mathcal{P}_{\chi}^{\text{ext}} + \delta_* \mathcal{P}_{\chi}^{\text{int}}$$

- 2 Path-independent virtual kinetic power

$$\begin{aligned} \delta_* \dot{\mathcal{T}}_{\chi}(\dot{\chi}, \dot{\mathbf{v}}_{\chi}, \dot{\mathbf{p}}_{\chi}) := & \int_{\mathcal{B}_0} \delta_* \dot{\mathbf{v}}_{\chi} \cdot (\rho_0 [(l_{\chi}^2 - l_0^2) \mathbf{A}_0 + l_0^2 \mathbf{I}] \mathbf{v}_{\chi} - \mathbf{p}_{\chi}) dV \\ & + \int_{\mathcal{B}_0} \delta_* \dot{\mathbf{p}}_{\chi} \cdot [\dot{\chi} - \mathbf{v}_{\chi}] dV + \int_{\mathcal{B}_0} \delta_* \dot{\chi} \cdot \dot{\mathbf{p}}_{\chi} dV \end{aligned}$$

- 3 Path-dependent virtual external power

$$\delta_* \dot{I}_{\chi}^{\text{ext}}(\dot{\alpha}, \dot{\chi}, \dot{\mathbf{Z}}, \dot{\tilde{\tau}}_n, \dot{\tilde{\nu}}) =: \delta_* \mathcal{P}_{\chi}^{\text{ext}}$$

where

$$\begin{aligned} \delta_* \mathcal{P}_{\chi}^{\text{ext}} := & - \int_{\mathcal{B}_0} \delta_* \dot{\chi} \cdot \mathbf{B}_{\chi} dV - \int_{\partial_W \mathcal{B}_0} \delta_* \dot{\chi} \cdot \bar{\mathbf{W}} dA - \int_{\partial_{\chi} \mathcal{B}_0} \delta_* \dot{\mathbf{Z}} \cdot [\dot{\chi} - \dot{\tilde{\chi}}] dA - \int_{\partial_{\chi} \mathcal{B}_0} \delta_* \dot{\chi} \cdot \bar{\mathbf{Z}} dA \\ & - \int_{\partial_{\chi} \mathcal{B}_0} 2 \delta_* \dot{\tilde{\tau}}_n \cdot \dot{\tilde{\nu}} dA - \int_{\partial_{\chi} \mathcal{B}_0} 2 \delta_* \dot{\tilde{\nu}} \cdot \dot{\tilde{\tau}}_n dA + \int_{\mathcal{B}_0} 2 \delta_* \dot{\alpha} \cdot \boldsymbol{\Sigma}_{\chi} dV \end{aligned}$$

Variational-based weak formulation (IV)

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

Virtual power associated with the reorientation (II)

Path-independent virtual internal power

$$\delta_* \dot{\Pi}_\chi^{\text{int}}(\dot{\alpha}, \dot{\chi}, \dot{\bar{\mathbf{F}}}_\chi, \dot{\bar{\mathbf{F}}}_\chi, \dot{\bar{\mathbf{G}}}_\chi, \dot{\bar{\mathbf{C}}}_\chi, \dot{\bar{\mathbf{K}}}_\chi, \dot{\bar{\boldsymbol{\tau}}}_n, \dot{\bar{\mathbf{P}}}_\chi, \dot{\bar{\mathbf{P}}}_K, \dot{\bar{\mathbf{S}}}_\chi, \dot{\bar{\mathbf{S}}}_K) := \delta_* \mathcal{P}_\chi^{\text{int}}$$

where

$$\begin{aligned} \delta_* \mathcal{P}_\chi^{\text{int}} &:= \int_{\mathcal{B}_0} \delta_* \dot{\bar{\mathbf{F}}}_\chi : [\bar{\mathbf{F}}_\chi \bar{\mathbf{S}}_\chi^t + \bar{\mathbf{G}}_\chi \bar{\mathbf{S}}_K^t] dV + \int_{\mathcal{B}_0} 2 \delta_* \dot{\bar{\boldsymbol{\tau}}}_n \cdot [\dot{\chi} + \boldsymbol{\epsilon} \cdot \dot{\alpha} \cdot \chi] dV \\ &+ \int_{\mathcal{B}_0} \delta_* \dot{\bar{\mathbf{P}}}_\chi : [\dot{\chi} \otimes \mathbf{n}_0 - \dot{\bar{\mathbf{F}}}_\chi] dV + \int_{\mathcal{B}_0} \delta_* \dot{\bar{\mathbf{P}}}_K : [\text{Grad}[\dot{\chi}] - \dot{\bar{\mathbf{G}}}_\chi] dV \\ &+ \int_{\mathcal{B}_0} \delta_* \dot{\bar{\mathbf{S}}}_\chi : \left[\frac{\partial}{\partial t} (\bar{\mathbf{F}}^t \bar{\mathbf{F}}_\chi) - \dot{\bar{\mathbf{C}}}_\chi \right] dV + \int_{\mathcal{B}_0} \delta_* \dot{\bar{\mathbf{S}}}_K : \left[\frac{\partial}{\partial t} (\bar{\mathbf{F}}^t \bar{\mathbf{G}}_\chi) - \dot{\bar{\mathbf{K}}}_\chi \right] dV \\ &+ \int_{\mathcal{B}_0} \delta_* \dot{\bar{\mathbf{C}}}_\chi : \left[\frac{\partial \Psi}{\partial \bar{\mathbf{C}}_\chi} - \bar{\mathbf{S}}_\chi \right] dV + \int_{\mathcal{B}_0} \delta_* \dot{\bar{\mathbf{K}}}_\chi : \left[\frac{\partial \Psi}{\partial \bar{\mathbf{K}}_\chi} - \bar{\mathbf{S}}_K \right] dV \\ &+ \int_{\mathcal{B}_0} \delta_* \dot{\bar{\mathbf{F}}}_\chi : [\bar{\mathbf{F}} \bar{\mathbf{S}}_\chi - \bar{\mathbf{P}}_\chi] dV + \int_{\mathcal{B}_0} \delta_* \dot{\bar{\mathbf{G}}}_\chi : [\bar{\mathbf{F}} \bar{\mathbf{S}}_K - \bar{\mathbf{P}}_K] dV \\ &+ \int_{\mathcal{B}_0} \dot{\bar{\mathbf{P}}}_\chi : [\delta_* \dot{\chi} \otimes \mathbf{n}_0] dV + \int_{\mathcal{B}_0} \dot{\bar{\mathbf{P}}}_K : \text{Grad}[\delta_* \dot{\chi}] dV + \int_{\mathcal{B}_0} \delta_* \dot{\bar{\mathbf{S}}}_\chi : \bar{\mathbf{F}}^t (\boldsymbol{\epsilon} \cdot \alpha) \bar{\mathbf{F}}_\chi dV \\ &+ \int_{\mathcal{B}_0} \left[\frac{1}{2} \boldsymbol{\epsilon} : \boldsymbol{\tau}_\chi - \dot{\bar{\boldsymbol{\tau}}}_n \cdot \boldsymbol{\epsilon} \cdot \chi \right] \cdot 2 \delta_* \dot{\alpha} dV + \int_{\mathcal{B}_0} 2 \dot{\bar{\boldsymbol{\tau}}}_n \cdot \delta_* \dot{\chi} dV \end{aligned}$$

Total virtual power in the incremental principle

$$\int_{\mathcal{I}_n} [\delta_* \mathcal{P}_\varphi + \delta_* \mathcal{P}_\Theta + \delta_* \dot{\mathcal{T}}_\chi(\dot{\chi}, \dot{\mathbf{v}}_\chi, \dot{\mathbf{p}}_\chi) + \delta_* \mathcal{P}_\chi^{\text{ext}} + \delta_* \mathcal{P}_\chi^{\text{int}}] dt = 0$$

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

Weak balance of linear momentum

$$\int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \delta_* \dot{\varphi} \cdot [\dot{\mathbf{p}} - \mathbf{B}] dV dt - \int_{\mathcal{I}_n} \int_{\partial_T \mathcal{B}_0} \delta_* \dot{\varphi} \cdot \bar{\mathbf{T}} dA dt + \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \text{Grad}[\delta_* \dot{\varphi}] : \tilde{\mathbf{P}} dV dt = \int_{\mathcal{I}_n} \int_{\partial_\varphi \mathcal{B}_0} \delta_* \dot{\varphi} \cdot \tilde{\mathbf{R}} dA dt$$

Weak balance of thermal momentum

(cf. Romero [2010], Schiebl & Betsch [2021])

$$\int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \delta_* \tilde{\Theta} \left[\dot{\eta} - \frac{D^{\text{tot}}}{\Theta} \right] dV dt - \int_{\mathcal{I}_n} \int_{\partial_Q \mathcal{B}_0} \delta_* \tilde{\Theta} \frac{\bar{\mathbf{Q}}}{\Theta} dA dt - \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \text{Grad}[\delta_* \tilde{\Theta}] \cdot \frac{1}{\Theta} \mathbf{Q} dV dt = \int_{\mathcal{I}_n} \int_{\partial_\Theta \mathcal{B}_0} \delta_* \tilde{\Theta} \tilde{\lambda} dA dt$$

Weak balance of orientational momentum

$$\int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \delta_* \dot{\chi} \cdot [\dot{\mathbf{p}}_\chi + 2 \tilde{\boldsymbol{\tau}}_n - \mathbf{B}_\chi] dV dt - \int_{\mathcal{I}_n} \int_{\partial_W \mathcal{B}_0} \bar{\mathbf{W}} \cdot \delta_* \dot{\chi} dA dt + \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \tilde{\mathbf{P}}_K : \text{Grad}[\delta_* \dot{\chi}] dV dt + \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \tilde{\mathbf{P}}_\chi : [\delta_* \dot{\chi} \otimes \mathbf{n}_0] dV dt = \int_{\mathcal{I}_n} \int_{\partial_\chi \mathcal{B}_0} \tilde{\mathbf{Z}} \cdot \delta_* \dot{\chi} dA dt$$

Weak balance of orientation rate

$$\int_{\mathcal{I}_n} \int_{\mathcal{B}_0} 2 \delta_* \tilde{\boldsymbol{\tau}}_n \cdot [\dot{\chi} + \boldsymbol{\epsilon} \cdot \dot{\boldsymbol{\alpha}} \cdot \chi] dV dt = \int_{\mathcal{I}_n} \int_{\partial_\chi \mathcal{B}_0} 2 \delta_* \tilde{\boldsymbol{\tau}}_n \cdot \tilde{\boldsymbol{\nu}} dA dt$$

Balance laws of the weak formulation (I)

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

Energy and momentum functions of the LCE extended continuum

Kinetic energy $\mathcal{T}(t) := \int_{\mathcal{B}_0} \frac{1}{2} \mathbf{v} \cdot \mathbf{p} \, dV$	Kinetic energy of orientation $\mathcal{T}_\chi(t) := \int_{\mathcal{B}_0} \frac{1}{2} \mathbf{v}_\chi \cdot \mathbf{p}_\chi \, dV$	Potential energy $\Pi^{\text{int}}(t) := \int_{\mathcal{B}_0} \Psi \, dV$
Linear momentum $\mathbf{L}(t) := \int_{\mathcal{B}_0} \mathbf{p} \, dV$	Angular momentum $\mathbf{J}(t) := \int_{\mathcal{B}_0} \boldsymbol{\varphi} \times \mathbf{p} \, dV$	Momentum of orientation $\mathbf{L}_\chi(t) := \int_{\mathcal{B}_0} \mathbf{p}_\chi \, dV$
Moment of momentum $\mathbf{J}_\chi(t) := \int_{\mathcal{B}_0} \boldsymbol{\chi} \times \mathbf{p}_\chi \, dV$	Reorientation function $\mathcal{C}^{\text{ori}}(t) := \int_{\mathcal{B}_0} [\ \boldsymbol{\chi}\ ^2 - 1] \, dV$	Thermal energy $\Pi^{\text{the}}(t) := \int_{\mathcal{B}_0} \Theta \eta \, dV$
Entropy $\mathcal{S}(t) := \int_{\mathcal{B}_0} \eta \, dV$	Total energy $\mathcal{H} := \mathcal{T} + \mathcal{T}_\chi + \Pi^{\text{int}} + \Pi^{\text{the}} + \Pi^{\text{ext}}$	Lyapunov function $\mathcal{F} := \mathcal{H} - \Theta_\infty \mathcal{S}$

Linear momentum

(symmetry of virtual translations)

$$\mathbf{L}(t_{n+1}) - \mathbf{L}(t_n) = \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \mathbf{B} \, dV dt + \int_{\mathcal{I}_n} \int_{\partial_T \mathcal{B}_0} \bar{\mathbf{T}} \, dA dt + \int_{\mathcal{I}_n} \int_{\partial_\varphi \mathcal{B}_0} \tilde{\mathbf{R}} \, dA dt$$

Orientalational momentum

(symmetry of virtual orientations)

$$\mathbf{L}_\chi(t_{n+1}) - \mathbf{L}_\chi(t_n) = \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} [\mathbf{B}_\chi - 2\tilde{\boldsymbol{\tau}}_n - \tilde{\mathbf{P}}_\chi \mathbf{n}_0] \, dV dt + \int_{\mathcal{I}_n} \int_{\partial_W \mathcal{B}_0} \bar{\mathbf{W}} \, dA dt + \int_{\mathcal{I}_n} \int_{\partial_\chi \mathcal{B}_0} \tilde{\mathbf{Z}} \, dA dt$$

Balance laws of the weak formulation (II)

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

Thermal momentum

(cf. Romero [2010], Schiebl & Betsch [2021])

$$\mathcal{S}(t_{n+1}) - \mathcal{S}(t_n) = \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \frac{D^{\text{tot}}}{\Theta} dV dt + \int_{\mathcal{I}_n} \int_{\partial_Q \mathcal{B}_0} \frac{\bar{Q}}{\Theta} dA dt + \int_{\mathcal{I}_n} \int_{\partial_\Theta \mathcal{B}_0} \tilde{\lambda} dA dt$$

Angular momentum

(symmetry of virtual rotations)

$$\begin{aligned} \mathbf{J}(t_{n+1}) - \mathbf{J}(t_n) &= \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \boldsymbol{\varphi} \times \mathbf{B} dV dt + \int_{\mathcal{I}_n} \int_{\partial_T \mathcal{B}_0} \boldsymbol{\varphi} \times \bar{\mathbf{T}} dA dt + \int_{\mathcal{I}_n} \int_{\partial_\varphi \mathcal{B}_0} \boldsymbol{\varphi} \times \tilde{\mathbf{R}} dA dt \\ &+ \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} [\tilde{\mathbf{F}}_\chi \tilde{\mathbf{S}}_\chi^t + \tilde{\mathbf{G}}_\chi \tilde{\mathbf{S}}_K^t] \times \tilde{\mathbf{F}} dV dt \end{aligned}$$

Moment of orientational momentum

(symmetry of virtual reorientations)

$$\begin{aligned} \mathbf{J}_\chi(t_{n+1}) - \mathbf{J}_\chi(t_n) &= \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \boldsymbol{\chi} \times \mathbf{B}_\chi dV dt + \int_{\mathcal{I}_n} \int_{\partial_W \mathcal{B}_0} \boldsymbol{\chi} \times \bar{\mathbf{W}} dA dt + \int_{\mathcal{I}_n} \int_{\partial_\chi \mathcal{B}_0} \boldsymbol{\chi} \times \tilde{\mathbf{Z}} dA dt \\ &- \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} [\tilde{\mathbf{F}}_\chi \tilde{\mathbf{S}}_\chi^t + \tilde{\mathbf{G}}_\chi \tilde{\mathbf{S}}_K^t] \times \tilde{\mathbf{F}} dV dt - \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \boldsymbol{\chi} \times 2\tilde{\boldsymbol{\tau}}_n dV dt \end{aligned}$$

Kinetic energy of motion

(symmetry of virtual time shifts)

$$\begin{aligned} \mathcal{T}(t_{n+1}) - \mathcal{T}(t_n) &= \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \mathbf{B} \cdot \dot{\boldsymbol{\varphi}} dV dt + \int_{\mathcal{I}_n} \int_{\partial_T \mathcal{B}_0} \bar{\mathbf{T}} \cdot \dot{\boldsymbol{\varphi}} dA dt + \int_{\mathcal{I}_n} \int_{\partial_\varphi \mathcal{B}_0} \tilde{\mathbf{R}} \cdot \dot{\boldsymbol{\varphi}} dA dt \\ &- \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} [\tilde{\mathbf{S}} : \dot{\tilde{\mathbf{F}}} + \tilde{\mathbf{S}}_\chi : \dot{\tilde{\mathbf{F}}}_\chi + \tilde{\mathbf{S}}_K : \dot{\tilde{\mathbf{F}}}_K] dV dt \end{aligned}$$



Balance laws of the weak formulation (III)

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

Kinetic energy of orientation

(symmetry of virtual time shifts)

$$\begin{aligned} \mathcal{T}_\chi(t_{n+1}) - \mathcal{T}_\chi(t_n) &= \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \mathbf{B}_\chi \cdot \dot{\chi} \, dV dt + \int_{\mathcal{I}_n} \int_{\partial_\varphi \mathcal{B}_0} \bar{\mathbf{W}} \cdot \dot{\chi} \, dA dt + \int_{\mathcal{I}_n} \int_{\partial_\varphi \mathcal{B}_0} \bar{\mathbf{Z}} \cdot \dot{\chi} \, dA dt \\ &\quad - \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} [\tilde{\mathbf{S}}_\chi : \tilde{\mathbf{F}}^t (\dot{\tilde{\mathbf{F}}}_\chi + \epsilon \cdot \dot{\alpha} \cdot \tilde{\mathbf{F}}_\chi) + \tilde{\mathbf{S}}_K : \tilde{\mathbf{F}}^t \dot{\tilde{\mathbf{G}}}_\chi + D_\chi^{\text{int}}] \, dV dt \end{aligned}$$

Thermal energy

(symmetry of virtual time shifts)

$$\begin{aligned} \Pi^{\text{the}}(t_{n+1}) - \Pi^{\text{the}}(t_n) &= \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} \left[-\frac{\partial \Psi}{\partial \Theta} \dot{\Theta} + D_\chi^{\text{int}} \right] \, dV dt + \int_{\mathcal{I}_n} \int_{\partial_\Theta \mathcal{B}_0} \dot{\Theta} \bar{h} \, dA dt \\ &\quad + \int_{\mathcal{I}_n} \int_{\partial_\Theta \mathcal{B}_0} \Theta \bar{\lambda} \, dA dt + \int_{\mathcal{I}_n} \int_{\partial_Q \mathcal{B}_0} \bar{Q} \, dA dt \end{aligned}$$

Potential energy

(symmetry of virtual time shifts)

$$\begin{aligned} \Pi(t_{n+1}) - \Pi(t_n) &= \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} [\tilde{\mathbf{S}}_\chi : \frac{\partial}{\partial t} (\tilde{\mathbf{F}}^t \tilde{\mathbf{F}}_\chi) + \tilde{\mathbf{S}}_K : \frac{\partial}{\partial t} (\tilde{\mathbf{F}}^t \tilde{\mathbf{G}}_\chi) + \tilde{\mathbf{S}}_\chi : \tilde{\mathbf{F}}^t (\epsilon \cdot \dot{\alpha}) \tilde{\mathbf{F}}_\chi] \, dV dt \\ &\quad + \int_{\mathcal{I}_n} \int_{\mathcal{B}_0} [\tilde{\mathbf{S}} : \dot{\tilde{\mathbf{F}}}^t \tilde{\mathbf{F}} - \mathbf{B} \cdot \dot{\varphi} - \mathbf{B}_\chi \cdot \dot{\chi}] \, dV dt \end{aligned}$$

Path-independent volume dead loads

$$\Pi^{\text{ext}}(t) := - \int_{\mathcal{B}_0} \mathbf{B} \cdot \varphi \, dV dt - \int_{\mathcal{B}_0} \mathbf{B}_\chi \cdot \chi \, dV$$

Balance laws of the weak formulation (IV)

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

Total energy

(cf. Holzapfel [2000], Romero [2010], Schiebl & Betsch [2021])

$$\begin{aligned} \mathcal{H}(t_{n+1}) - \mathcal{H}(t_n) = & \int_{\mathcal{T}_n} \int_{\partial_\varphi \mathcal{B}_0} \tilde{\mathbf{R}} \cdot \dot{\boldsymbol{\varphi}} \, dA \, dt + \int_{\mathcal{T}_n} \int_{\partial_\chi \mathcal{B}_0} \tilde{\mathbf{Z}} \cdot \dot{\boldsymbol{\chi}} \, dA \, dt \\ & - \int_{\mathcal{T}_n} \int_{\partial_T \mathcal{B}_0} \tilde{\mathbf{T}} \cdot \dot{\boldsymbol{\varphi}} \, dA \, dt + \int_{\mathcal{T}_n} \int_{\partial_W \mathcal{B}_0} \tilde{\mathbf{W}} \cdot \dot{\boldsymbol{\chi}} \, dA \, dt \\ & - \int_{\mathcal{T}_n} \int_{\partial_\Theta \mathcal{B}_0} \tilde{\lambda} \Theta \, dA \, dt + \int_{\mathcal{T}_n} \int_{\partial_{\dot{\Theta}} \mathcal{B}_0} \tilde{h} \dot{\Theta} \, dA \, dt + \int_{\mathcal{T}_n} \int_{\partial_Q \mathcal{B}_0} \bar{Q} \, dA \, dt \end{aligned}$$

Lyapunov function

(cf. Romero [2010], Schiebl & Betsch [2021])

$$\begin{aligned} \mathcal{F}(t_{n+1}) - \mathcal{F}(t_n) = & \int_{\mathcal{T}_n} \int_{\partial_T \mathcal{B}_0} \tilde{\mathbf{T}} \cdot \dot{\boldsymbol{\varphi}} \, dA \, dt + \int_{\mathcal{T}_n} \int_{\partial_\varphi \mathcal{B}_0} \tilde{\mathbf{R}} \cdot \dot{\boldsymbol{\varphi}} \, dA \, dt \\ & + \int_{\mathcal{T}_n} \int_{\partial_W \mathcal{B}_0} \tilde{\mathbf{W}} \cdot \dot{\boldsymbol{\chi}} \, dA \, dt + \int_{\mathcal{T}_n} \int_{\partial_\chi \mathcal{B}_0} \tilde{\mathbf{Z}} \cdot \dot{\boldsymbol{\chi}} \, dA \, dt + \int_{\mathcal{T}_n} \int_{\partial_{\dot{\Theta}} \mathcal{B}_0} \tilde{h} \dot{\Theta} \, dA \, dt \\ & - \int_{\mathcal{T}_n} \int_{\mathcal{B}_0} \frac{\Theta - \Theta_\infty}{\Theta} D^{\text{tot}} \, dV \, dt + \int_{\mathcal{T}_n} \int_{\partial_Q \mathcal{B}_0} \frac{\Theta - \Theta_\infty}{\Theta} \bar{Q} \, dA \, dt \end{aligned}$$

Reorientation function

(cf. Betsch & Steinmann [2002])

$$\mathcal{C}^{\text{ori}}(t_{n+1}) - \mathcal{C}^{\text{ori}}(t_n) \equiv \int_{\mathcal{T}_n} \int_{\mathcal{B}_0} 2 \boldsymbol{\chi} \cdot \dot{\boldsymbol{\chi}} \, dV \, dt = \int_{\mathcal{T}_n} \int_{\partial_\chi \mathcal{B}_0} 2 \boldsymbol{\chi} \cdot \tilde{\boldsymbol{\nu}} \, dA \, dt$$

Thin LCE strip subject to initial rotation

Boundary and initial conditions

121-em with H2O-mixed-Bbar

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

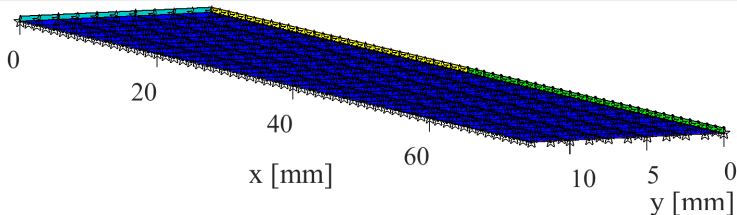
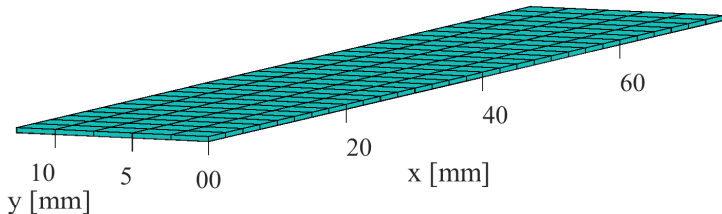
Temperature control

Transient heat flux load

Summary

Mesh and boundary conditions

$$n_0^A = e_y, \omega_0^A = 32 e_z [1/s]$$



Activated Dirichlet and Neumann boundaries

Blue bottom as $\partial_x \mathcal{B}_0 \equiv \partial_\theta \mathcal{B}_0$: Fixed orientation $n_z^A = 0$ and temperature $\theta^A = \theta_\infty$



Thin LCE strip subject to initial rotation

Unsteady right-left-rotation due to reorientation

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

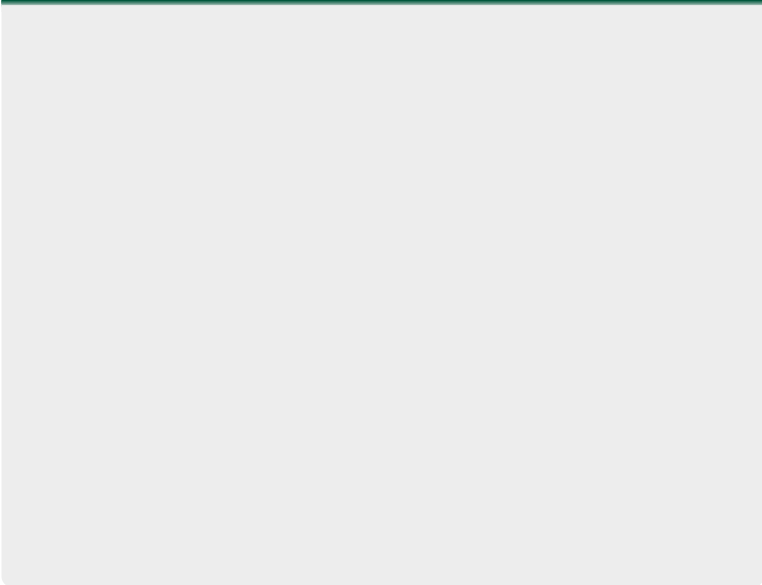
Temperature control

Transient heat flux load

Summary

Movie of a **soft** strip

($E \approx 0.914$ [MPa], $\nu \approx 0.493$)



Thin LCE film subject to initial rotation

Unsteady right-left-rotation due to reorientation

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

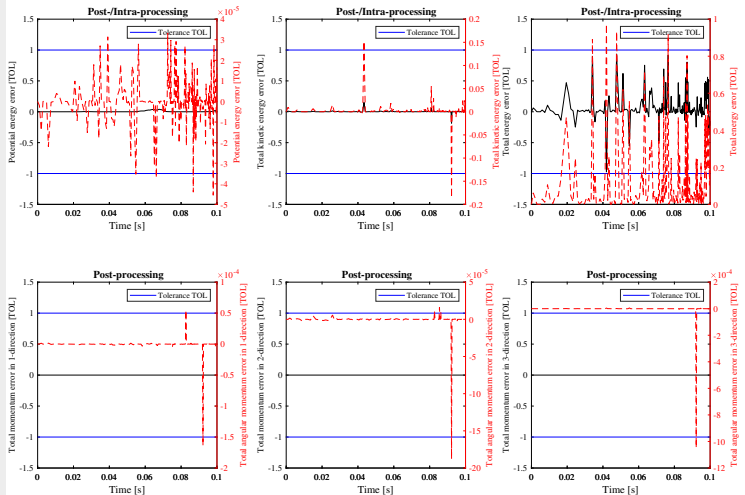
Temperature control

Transient heat flux load

Summary

Balance laws versus time

($E \approx 0.914$ [MPa], $\nu \approx 0.493$)





Thin LCE strip subject to temperature control

Boundary and initial conditions

121-em with H2O-mixed-Bbar

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

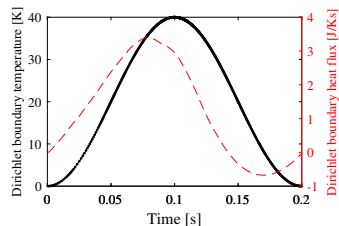
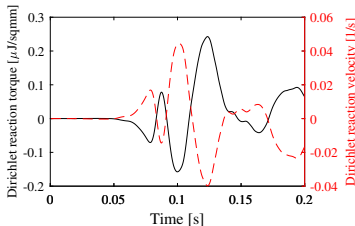
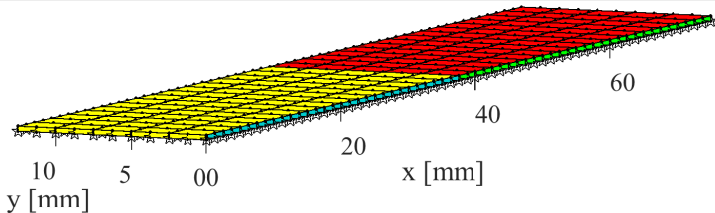
Temperature control

Transient heat flux load

Summary

Boundary conditions and loads

$$\theta_0 = \theta_\infty, \hat{\theta} = 40 \text{ [K]}$$



Activated Dirichlet and Neumann boundaries

Blue bottom as $\partial_\chi \mathcal{B}_0 \equiv \partial_\theta \mathcal{B}_0$: Fixed orientation $n_z^A = 0$ and temperature $\theta^A = \theta_\infty$

Yellow top as $\partial_\theta \mathcal{B}_0$: $\theta^A = \hat{\theta} f(t)$

Red top as boundary $\partial_Q \mathcal{B}_0$: thermally isolated



Thin LCE strip subject to temperature control

Bending motion in direction to the boundary normal of $\partial_\chi \mathcal{B}_0$

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

Movie of a **soft** strip

($\mathbf{n}_0 = \mathbf{e}_y$, $E \approx 0.914$ [MPa], $\nu \approx 0.493$)

Thin LCE strip subject to temperature control

Bending motion in direction to the boundary normal of $\partial_\chi \mathcal{B}_0$

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

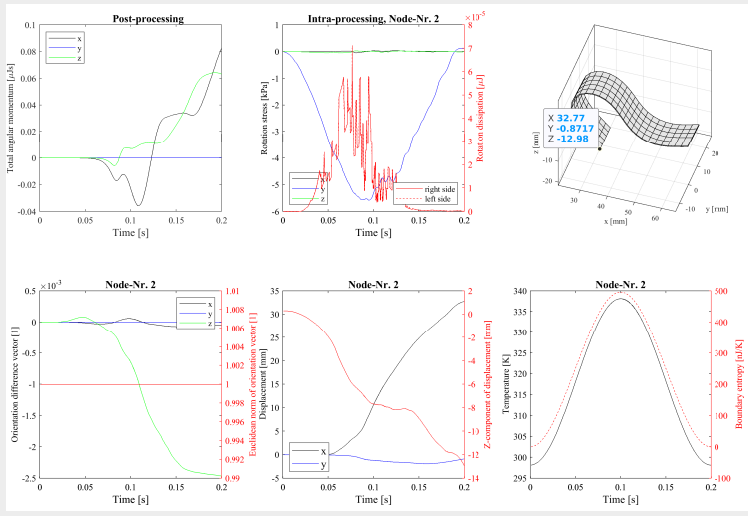
Temperature control

Transient heat flux load

Summary

Nodal time evolutions

$$(n_0 = e_y, E \approx 0.914 \text{ [MPa]}, \nu \approx 0.493)$$





Thin LCE strip subject to temperature control

Bending motion in direction to the boundary normal of $\partial_\chi \mathcal{B}_0$

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

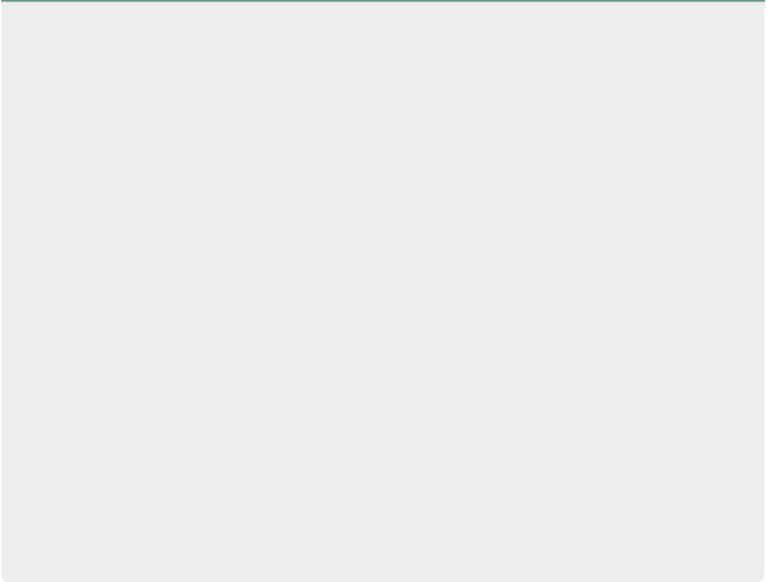
Temperature control

Transient heat flux load

Summary

Movie of a **soft** strip

($n_0 = e_x$, $E \approx 0.914$ [MPa], $\nu \approx 0.493$)





Thin LCE strip subject to transient heat flux load

Boundary and initial conditions

121-em with H2O-mixed-Bbar

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

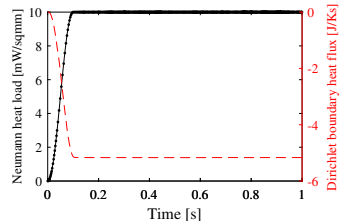
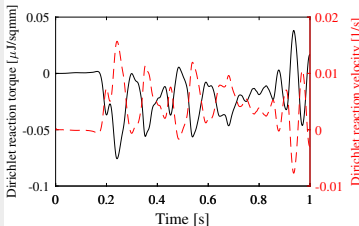
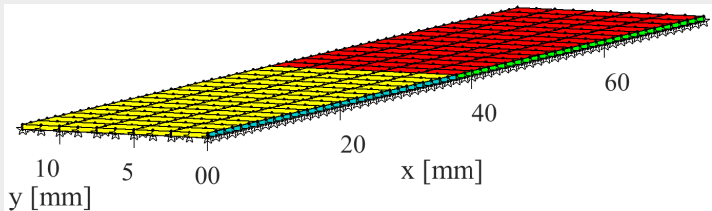
Temperature control

Transient heat flux load

Summary

Boundary conditions and loads

$$n_0 = e_y, \theta_0 = \theta_\infty$$



Activated Dirichlet and Neumann boundaries

Blue bottom as $\partial_x B_0 \equiv \partial_\theta B_0$: Fixed orientation $n_z^A = 0$ and temperature $\theta^A = \theta_\infty$

Yellow top as $\partial_\theta B_0$: $\theta^A = \theta_0$

Red top as boundary $\partial_Q B_0$: $\bar{Q} = \hat{Q} f_Q(t)$



Thin LCE strip subject to transient heat flux load

Bending motion in direction to the boundary normal of $\partial_x \mathcal{B}_0$

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

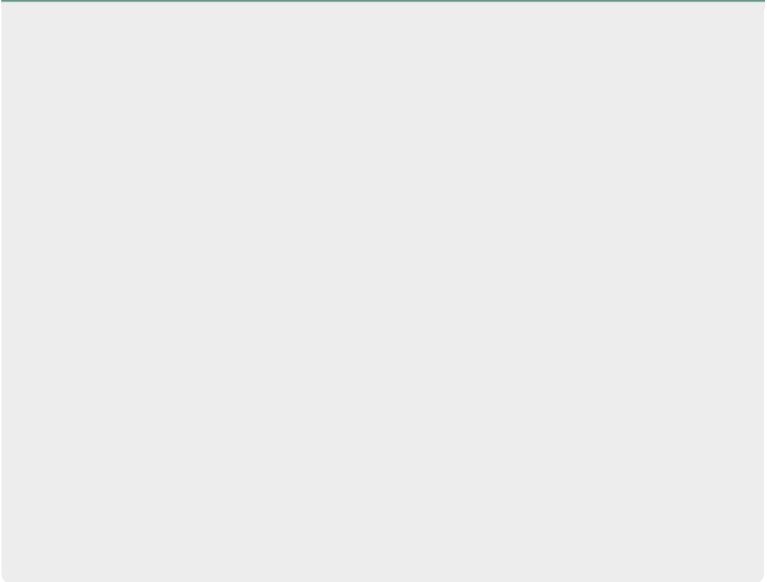
Temperature control

Transient heat flux load

Summary

Movie of a **soft** strip

($E \approx 0.914$ [MPa], $\nu \approx 0.493$)



Thin LCE strip subject to volume load

Bending motion in direction to the boundary normal of $\partial_x \mathcal{B}_0$

A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

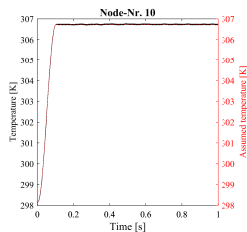
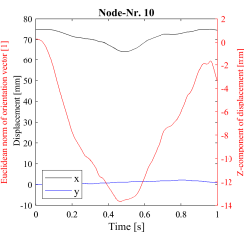
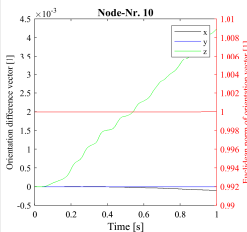
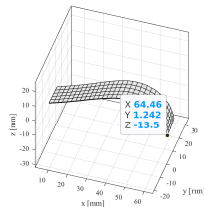
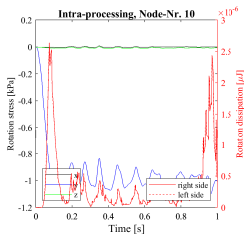
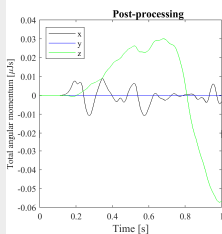
Initial rotation

Temperature control

Transient heat flux load

Summary

Nodal time evolutions and balance laws (E \approx 0.914 [MPa], $\nu \approx$ 0.493)



A new mixed finite element formulation for reorientation in liquid crystalline elastomers

Groß M., Dietzsch J. and Concas F.

Introduction

Continuum model

Reorientation

Variational-based weak formulation

Balance laws

Numerical studies

Initial rotation

Temperature control

Transient heat flux load

Summary

- 1 Aims: **Dynamic simulations of motion actuations**
 - ▶ of **liquid crystalline elastomers** by means of
 - ▶ **thermal Dirichlet** and **Neumann boundaries**.
- 2 Numerical goals: **Dynamic finite element simulations**
 - ▶ with the approach of a **mixed finite element** method and
 - ▶ **reorientations** by means of drilling degrees of freedom.
- 3 Numerical strategy:
 - ▶ introducing an **independent global orientation field**,
 - ▶ formulating local rotations by **drilling degrees of freedom**,
 - ▶ using **local evolution equations** for stress-induced motions.
- 4 Numerical results: **Motion actuations with**
 - ▶ thermal **Dirichlet** and **Neumann boundaries**
 - ▶ activating **bending motions** as in experiments.
- 5 Next steps:
 - ▶ **Simulation of UV light actuations** by **chemical processes**