

A mixed finite element formulation for energy-momentum time integrations of composites with fiber bending stiffness

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GAMM 2021 (Virtual congress)

17 March, 2021



DFG Deutsche
Forschungsgemeinschaft

Acknowledgments: This research is provided by DFG grant GR 3297/4 and 3297/6.

Motivation

- ▶ Dynamic simulations of fiber-reinforced materials in lightweight structures
- ▶ Keywords:
 - ▶ Nearly-incompressible material behavior
 - ▶ Anisotropic material behavior
 - ▶ Fiber stretch stiffness
 - ▶ Fiber bending stiffness
 - ▶ Long term simulations
- ▶ Solution strategy:
 1. Extend the Cauchy-Boltzmann continuum by higher order gradients to capture fiber bending stiffness
 2. Mixed finite elements to reduce locking effects
 3. Higher-order energy-momentum conserving time integrator for stable and accurate dynamic simulations

Continuum mechanics

[Asmanoglo 17]

- ▶ Deformation gradient F and right Cauchy-Green tensor $C = F^T F$
- ▶ Fiber direction a_0 and structural tensor $M = a_0^T \otimes a_0$
- ▶ Gradient of fiber direction $G = \nabla[a_0 \cdot F^T] = a_0 \cdot \nabla[F^T]$ for $a_0 = \text{const.}$
- ▶ Referential representation $\Lambda(F, \nabla[F]) = F^T \cdot a_0 \cdot \nabla[F]^{T12}$

Strain energy function

[Asmanoglo 17]

$$\Psi = \Psi_M^{\text{ISO}}(C, J) + \Psi_M^{\text{VOL}}(J) + \Psi_F^{\text{ANI}}(C, a_0) + \Psi_F^{\text{HOG}}(C, \Lambda)$$

- ▶ Isotropic part Ψ^{ISO} and Volumetric part Ψ^{VOL} of the matrix

$$I_1(C) = C : I \quad I_3(C) = \det[C] = J^2 \quad (I_2(C) = \text{cof}[C] : I)$$
- ▶ Anisotropic part Ψ^{ANI} regarding to the stretching of the fiber

$$I_4(C, a_0) = a_0 \cdot C \cdot a_0 \quad (I_5(C, a_0) = a_0 \cdot C^2 \cdot a_0)$$
- ▶ Anisotropic part Ψ^{HOG} regarding to the bending of the fiber

$$I_6 = \kappa_0 \cdot \kappa_0 \quad I_7 = \kappa_0 \cdot C \cdot \kappa_0 \quad \kappa_0 = \Lambda \cdot a_0$$

Total internal energy Π^{int} for the mixed principle of virtual power

[Groß 18]

$$\begin{aligned}
 \Pi^{\text{int}} = & \int_{\mathcal{B}_0} \frac{1}{2} \mathbf{S} : (\mathbf{C} - \tilde{\mathbf{C}}) dV + \int_{\mathcal{B}_0} \tilde{\mathbf{S}} : \tilde{\mathbf{C}} dV + \int_{\mathcal{B}_0} p (J(\tilde{\mathbf{C}}) - \tilde{J}) dV + \int_{\mathcal{B}_0} \tilde{p} \tilde{J} dV \\
 & + \int_{\mathcal{B}_0} \frac{1}{2} \mathbf{S}_A : (\tilde{\mathbf{C}} - \tilde{\mathbf{C}}_A) dV + \int_{\mathcal{B}_0} \tilde{\mathbf{S}}_A : \tilde{\mathbf{C}}_A dV + \int_{\mathcal{B}_0} \Psi dV \\
 & + \int_{\mathcal{B}_0} \mathbf{H} : (\mathbf{\Lambda}(\tilde{\mathbf{F}}, \tilde{\mathbf{\Gamma}}) - \tilde{\mathbf{\Lambda}}) dV + \int_{\mathcal{B}_0} \tilde{\mathbf{H}} : \tilde{\mathbf{\Lambda}} dV + \int_{\mathcal{B}_0} \mathbf{P} : (\mathbf{F} - \tilde{\mathbf{F}}) dV + \int_{\mathcal{B}_0} \mathbf{B} \odot_3 (\nabla(\tilde{\mathbf{F}}) - \tilde{\mathbf{\Gamma}}) dV \\
 \Psi = & \left[\Psi_{\text{M}}^{\text{ISO}}(\tilde{\mathbf{C}}, \tilde{J}) + \Psi_{\text{M}}^{\text{VOL}}(\tilde{J}) + \Psi_{\text{F}}^{\text{ANI}}(\tilde{\mathbf{C}}_A, M) + \Psi_{\text{F}}^{\text{HOG}}(\tilde{\mathbf{C}}_A, \mathbf{\Lambda}) \right]
 \end{aligned}$$

- Independent mixed field $\tilde{\mathbf{C}}$ and corresponding Lagrangian multiplier \mathbf{S}
- Superimposed stress tensor $\tilde{\mathbf{S}}$ to derive energy–momentum scheme [Groß 18]
- Independent mixed fields $\tilde{\mathbf{F}}$ and $\tilde{\mathbf{\Gamma}}$ for \mathbf{F} and $\nabla(\mathbf{F})$ $\left(\mathbf{\Lambda}(\mathbf{F}, \nabla(\mathbf{F})) \rightarrow \mathbf{\Lambda}(\tilde{\mathbf{F}}, \tilde{\mathbf{\Gamma}}) \right)$
- Independent mixed field $\tilde{\mathbf{\Lambda}}$ for $\mathbf{\Lambda}(\tilde{\mathbf{F}}, \tilde{\mathbf{\Gamma}})$ and corresponding superimposed field $\tilde{\mathbf{H}}$ for energy–momentum scheme
- Independent mixed fields for the volumetric dilatation \tilde{J} and $\tilde{\mathbf{C}}_A$ for the anisotropic part of the strain energy function [Simo 85] [Schr 16]

Superimposed fields

[Groß 18] [Groß 20]

$$\begin{aligned}
 \tilde{S} &= \frac{\tilde{\Psi}(1) - \tilde{\Psi}(0) - \int \frac{\partial \tilde{\Psi}}{\partial \dot{\mathbf{C}}} : \dot{\mathbf{C}}}{\dot{\mathbf{C}} : \dot{\mathbf{C}}} \dot{\mathbf{C}} & \tilde{p} &= \frac{\tilde{\Psi}(1) - \tilde{\Psi}(0) - \int \frac{\partial \tilde{\Psi}}{\partial \dot{J}} \dot{J}}{\dot{J} \dot{J}} \dot{J} \\
 \tilde{S}_A &= \frac{\tilde{\Psi}(1) - \tilde{\Psi}(0) - \int \frac{\partial \tilde{\Psi}}{\partial \dot{\mathbf{C}}_A} : \dot{\mathbf{C}}_A}{\dot{\mathbf{C}}_A : \dot{\mathbf{C}}_A} \dot{\mathbf{C}}_A & \tilde{H} &= \frac{\tilde{\Psi}(1) - \tilde{\Psi}(0) - \int \frac{\partial \tilde{\Psi}}{\partial \dot{\mathbf{\Lambda}}} : \dot{\mathbf{\Lambda}}}{\dot{\mathbf{\Lambda}} : \dot{\mathbf{\Lambda}}} \dot{\mathbf{\Lambda}}
 \end{aligned}$$

Mixed principle of virtual power

▶ Total power functional

$$\dot{T} + \dot{\Pi}^{\text{ext}} + \dot{\Pi}^{\text{int}} = \dot{\mathcal{H}}(\dot{\mathbf{q}}, \dot{\mathbf{v}}, \dot{\mathbf{p}}, \dot{\lambda}_q, \dot{\mathbf{C}}, \dot{J}, \dot{\mathbf{C}}_A, \dot{\mathbf{F}}, \dot{\mathbf{\Gamma}}, \dot{\mathbf{\Lambda}}, S, p, S_A, P, B, H)$$

▶ Kinetic power functional

$$\dot{T}(\dot{\mathbf{q}}, \dot{\mathbf{v}}, \dot{\mathbf{p}}) = \int_{\mathcal{B}_0} (\rho_0 \mathbf{v} - \mathbf{p}) \cdot \dot{\mathbf{v}} dV + \int_{\mathcal{B}_0} \dot{\mathbf{p}} \cdot (\dot{\mathbf{q}} - \mathbf{v}) dV + \int_{\mathcal{B}_0} \mathbf{p} \cdot \ddot{\mathbf{q}} dV$$

▶ External power functional

$$\dot{\Pi}^{\text{ext}}(\dot{\mathbf{q}}, \dot{\lambda}_q) = - \int_{\partial \mathcal{B}_0} \mathbf{t} \cdot \dot{\mathbf{q}} dA - \int_{\partial \mathcal{B}_0} \dot{\lambda}_q \cdot (\dot{\mathbf{q}} - \dot{\mathbf{q}}^{\text{ref}}) dA$$

Variation with respect to the variables in the arguments of the total energy balance

$$\int_T \delta_* \dot{\mathcal{H}} dt = \int_T [\delta_* \dot{T} + \delta_* \dot{\Pi}^{\text{ext}} + \delta_* \dot{\Pi}^{\text{int}}] dt = 0$$

Weak forms

$$\int_T \int_{\mathcal{B}_0} \left[\mathbf{S} : \frac{1}{2} \frac{\partial \dot{\mathbf{C}}}{\partial \dot{\mathbf{q}}} + \mathbf{P} : \frac{\partial \dot{\mathbf{F}}}{\partial \dot{\mathbf{q}}} - \dot{\mathbf{p}} \right] \cdot \delta_* \dot{\mathbf{q}} dV dt = 0 \quad \int_T \int_{\partial \mathcal{B}_0} [-\mathbf{t} - \boldsymbol{\lambda}_q] \cdot \delta_* \dot{\mathbf{q}} dA dt = 0$$

$$\int_T \int_{\mathcal{B}_0} \left[\frac{1}{\rho_0} \mathbf{p} - \dot{\mathbf{q}} \right] \cdot \delta_* \dot{\mathbf{v}} dV dt = 0 \quad \int_T \int_{\partial \mathcal{B}_0} [\dot{\mathbf{q}} - \dot{\mathbf{q}}^{\text{ref}}(t)] \cdot \delta_* \boldsymbol{\lambda}_q dA dt = 0$$

$$\int_T \int_{\mathcal{B}_0} \left[\frac{1}{2} \mathbf{S} - \left(\frac{\partial \Psi}{\partial \dot{\mathbf{C}}} + \dot{\mathbf{S}} + \frac{p}{2J} \text{cof}[\mathbf{C}] + \frac{1}{2} \mathbf{S}_A \right) \right] : \delta_* \dot{\mathbf{C}} dV dt = 0 \quad \int_T \int_{\mathcal{B}_0} \left[p - \left[\frac{\partial \Psi}{\partial \dot{J}} + \dot{p} \right] \right] \delta_* \dot{J} dV dt = 0$$

$$\int_T \int_{\mathcal{B}_0} \left[\frac{1}{2} \mathbf{S}_A - \left(\frac{\partial \Psi}{\partial \dot{\mathbf{C}}_A} + \dot{\mathbf{S}}_A \right) \right] : \delta_* \dot{\mathbf{C}}_A dV dt = 0 \quad \int_T \int_{\mathcal{B}_0} \left[\mathbf{P} - \left(\mathbf{H} : \frac{\partial \dot{\mathbf{\Lambda}}}{\partial \dot{\mathbf{F}}} + \mathbf{B} : \frac{\partial \nabla \dot{\mathbf{F}}}{\partial \dot{\mathbf{F}}} \right) \right] : \delta_* \dot{\mathbf{F}} dV dt$$

$$\int_T \int_{\mathcal{B}_0} \left[\mathbf{B} - \mathbf{H} : \frac{\partial \dot{\mathbf{\Lambda}}}{\partial \dot{\mathbf{\Gamma}}} \right] : \delta_* \dot{\mathbf{\Gamma}} dV dt = 0 \quad \int_T \int_{\mathcal{B}_0} \left[\mathbf{H} - \left[\frac{\partial \Psi}{\partial \dot{\mathbf{\Lambda}}} + \dot{\mathbf{H}} \right] \right] \delta_* \dot{\mathbf{\Lambda}} dV dt = 0$$

$$\int_T \int_{\mathcal{B}_0} \frac{1}{2} [\dot{\mathbf{C}} - \dot{\mathbf{C}}] : \delta_* \mathbf{S} dV dt = 0 \quad \int_T \int_{\mathcal{B}_0} [\dot{\mathbf{J}} - \dot{J}] \delta_* p dV dt = 0 \quad \int_T \int_{\mathcal{B}_0} \frac{1}{2} [\dot{\mathbf{C}}_A - \dot{\mathbf{C}}] : \delta_* \mathbf{S}_A dV dt = 0$$

$$\int_T \int_{\mathcal{B}_0} [\dot{\mathbf{F}} - \dot{\mathbf{F}}] : \delta_* \mathbf{P} dV dt = 0 \quad \int_T \int_{\mathcal{B}_0} [\nabla(\dot{\mathbf{F}}) - \dot{\mathbf{\Gamma}}] \odot_3 \delta_* \mathbf{B} dV dt = 0 \quad \int_T \int_{\mathcal{B}_0} [\dot{\mathbf{\Lambda}} - \dot{\mathbf{\Lambda}}] : \delta_* \mathbf{H} dV dt = 0$$

Approximation

k = Polynomial degree in time

- ▶ Discretization in space and time
- ▶ Lagrangian shape functions in space (N) [Wrig 08] [Bart 18]
 - ▶ Independent approximation of the different mixed fields
 - ▶ Lagrangian multiplier approximated equally as the corresponding mixed fields e.g. \tilde{C}_A & S_A or \tilde{J} & p
- ▶ Lagrangian shape functions in time (M, M', \tilde{M}) [Bets 01] [Groß 18]

$$M_i(\alpha) = \prod_{\substack{j=1 \\ j \neq i}}^{k+1} \frac{\alpha - \alpha_j}{\alpha_i - \alpha_j}, \quad 1 \leq i \leq k+1 \quad \tilde{M}_i(\alpha) = \prod_{\substack{j=1 \\ j \neq i}}^k \frac{\alpha - \alpha_j}{\alpha_i - \alpha_j}, \quad 1 \leq i \leq k$$

- ▶ Time rate variables and mixed fields ($q, v, p, \tilde{C}, \tilde{J}, \tilde{C}_A, \tilde{F}, \tilde{\Gamma}, \tilde{\Lambda}$)

$$(\bullet)^{e,h} = \sum_{I=1}^{k+1} \sum_{A=1}^{n_{no}} M_I(\alpha) N^A(\xi) (\bullet)_I^{eA} \quad \left(\dot{(\bullet)}^{e,h} = \frac{1}{h_n} \sum_{I=1}^{k+1} \sum_{A=1}^{n_{no}} M'_I(\alpha) N^A(\xi) (\bullet)_I^{eA} \right)$$

- ▶ Lagrangian multiplier and variation fields ($\lambda_q, S, p, S_A, P, B, H, \delta_* \bullet$)

$$(\bullet)^{e,h} = \sum_{I=1}^k \sum_{A=1}^{n_{nou}} \tilde{M}_I N^A(\bullet)_I^{eA}$$

Implementation

1. Staggered solution of mixed fields at element level, e.g.

- ▶ 1. Solve values of \tilde{J} with equation $\int_T \int_{\mathcal{B}_0} [\dot{\tilde{J}} - \dot{J}] \delta p dV dt = 0$
- ▶ 2. Solve values of p with \tilde{J} and equation $\int_T \int_{\mathcal{B}_0} \left[p - \left[\frac{\partial \Psi}{\partial \tilde{J}} + \tilde{p} \right] \right] \delta \tilde{J} dV dt = 0$

2. Eliminate \mathbf{p}

$$\int_T \int_{\mathcal{B}_0} \left[\mathbf{S} : \frac{1}{2} \frac{\partial \dot{\mathbf{C}}}{\partial \dot{\mathbf{q}}} + \mathbf{P} : \frac{\partial \dot{\mathbf{F}}}{\partial \dot{\mathbf{q}}} - \dot{\mathbf{p}} \right] \cdot \delta \dot{\mathbf{q}} dV dt = 0 \quad \int_T \int_{\mathcal{B}_0} \left[\frac{1}{\rho_0} \mathbf{p} - \dot{\mathbf{q}} \right] \cdot \delta \dot{\mathbf{v}} dV dt = 0$$

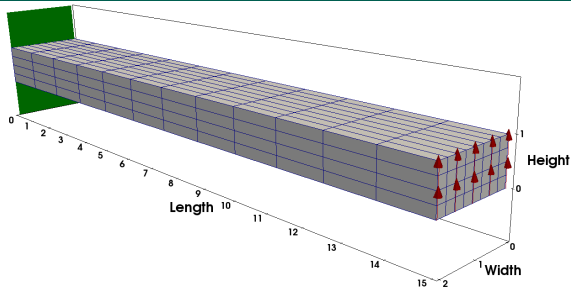
- ▶ Rearrange first equation to \mathbf{p} and insert in second equation

3. Condensate at element level to pure displacement temperature form

- ▶ Schur complements \Rightarrow All inverted matrices are constant

Angular momentum balance law

$$\begin{aligned} \mathcal{J}_{n+1} - \mathcal{J}_n = & \int_{t_n}^{t_{n+1}} \int_{\mathcal{B}_0} \left[\left(\mathbf{H} : \frac{\partial \dot{\mathbf{\Lambda}}}{\partial \dot{\mathbf{F}}} + \mathbf{B} : \frac{\partial \nabla \dot{\mathbf{F}}}{\partial \dot{\mathbf{F}}} \right) \times \tilde{\mathbf{F}} \right] dV dt + \int_{t_n}^{t_{n+1}} \int_{\partial \mathcal{B}_0} [\mathbf{q} \times \boldsymbol{\lambda}_q] dV dt \\ & + \int_{t_n}^{t_{n+1}} \int_{\partial \mathcal{B}_0} [\mathbf{q} \times \mathbf{t}] dV dt \end{aligned}$$

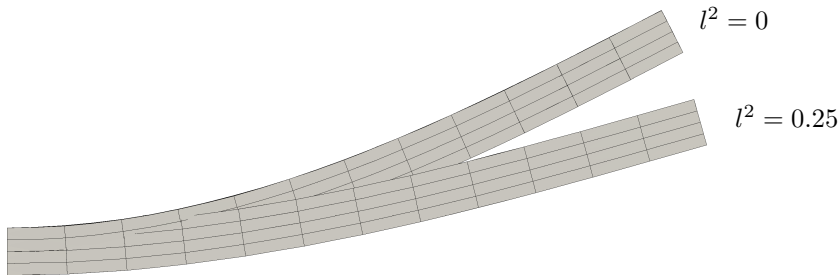


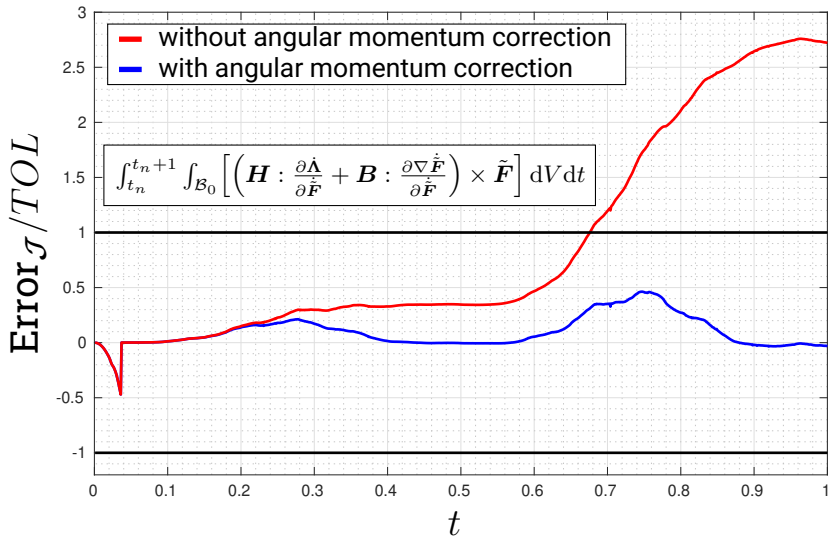
- Matrix part and fiber stretch part taken from [Dal 17]

$$\Psi^{\text{ISO}} = \frac{\epsilon_1}{2} (\text{tr}[\mathbf{C}] - 3 - 2\ln(J)) \quad \Psi^{\text{VOL}} = \frac{\epsilon_2}{2} \ln(J)^2 \quad \Psi^{\text{ANI}} = \frac{\epsilon_3}{2} (\text{tr}[\mathbf{CM}] - 1)^2$$

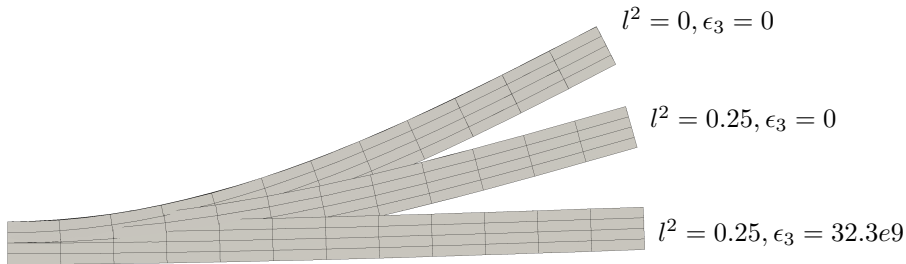
- Anisotropic direction $(\mathbf{a}_0)^T = [1 \ 0 \ 0]$
- $T = 1.0$, $h_n = 0.001$, $k = 1$ and $\hat{p} = 3.5e6 f_{\hat{p}}$ with $f_{\hat{p}} = \frac{1}{T}t$
- Quadratic serendipity mesh (20 nodes) with $n_{el} = 384$
- Linear approximation for \tilde{J} and constant approximation for \tilde{C}_A
- Introducing length scale l^2 with $c = \epsilon_1 l^2$ for material parameter of Ψ^{HOG}

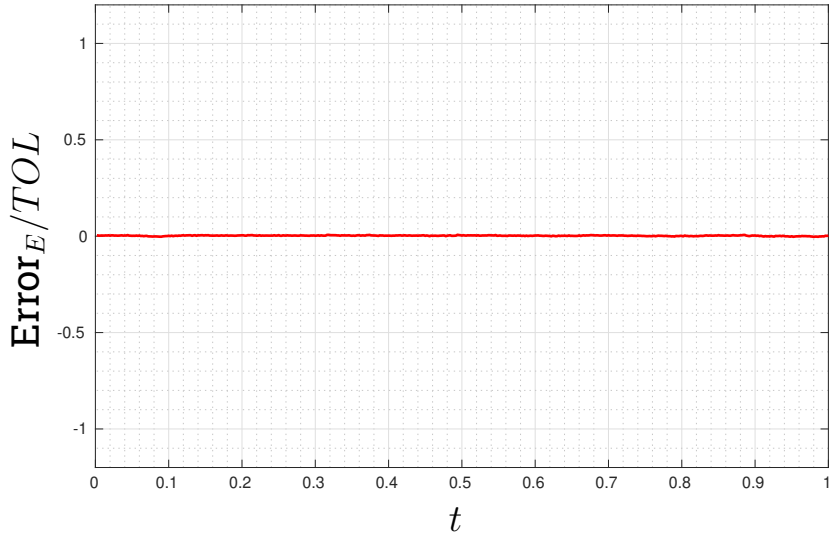
$$\Psi^{\text{HOG}} = \epsilon_1 l^2 I_6 \text{ [Asmanoglo 17]}$$



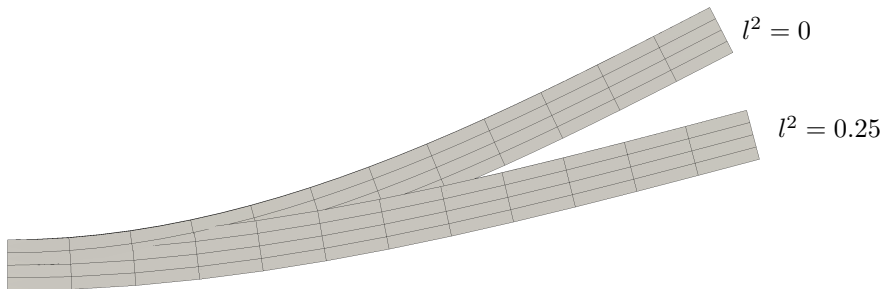


$$\Psi^{\text{HOG}} = \epsilon_1 l^2 I_6$$



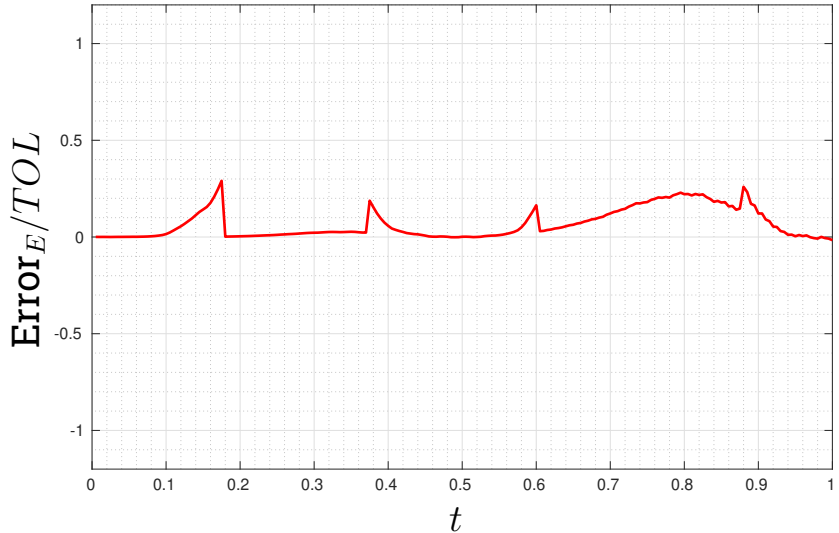


$$\Psi^{\text{HOG}} = \epsilon_1 l^2 (I_7 - I_6)^2 \text{ [Asmanoglo 17]}$$



Numerical example

Energy conservation $\epsilon_1 = 4.04e9$ $\epsilon_2 = 5.2e9$ $\epsilon_3 = 32.3e9$ $l^2 = 0.25$



Conclusion

- ▶ Motivation:
 - ▶ Dynamic simulations of fiber-reinforced materials in light-weight structures
- ▶ Important results:
 - ▶ Higher-order gradients capture the fiber-bending stiffness
 - ▶ Higher-order energy-momentum time integrators conserve total energy
- ▶ Outlook:
 - ▶ Extension of the material formulation to a thermo-viscoelastic formulation
 - ▶ Investigation of locking effects

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