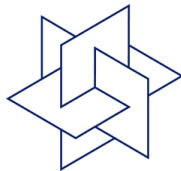


# Positive Real Balanced Truncation Model Reduction of Descriptor Systems

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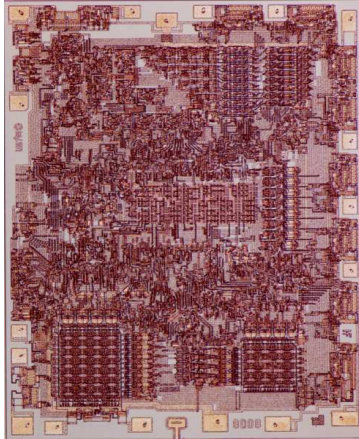
Joint work with Tatjana Stykel

*Workshop on Matrix Equations, Chemnitz, June 15, 2007*

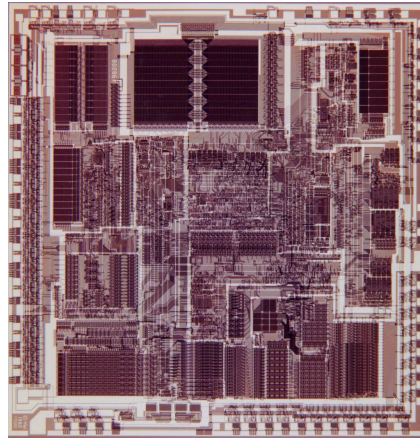
# Motivation



<http://www.intel.com>



1972: Intel 8008  
 $10\mu$ , 3.500 comp.  
800 KHz



1982: Intel 286  
 $1.5\mu$ , 134.000 comp.  
12 MHz, 2 km



2002: Intel Pentium 4  
 $0.13\mu$ ,  $55 \cdot 10^6$  comp.  
2.4 GHz, 4 km

- decrease of feature size
- increase of chip complexity
- increase of operation frequencies
- increase of interconnect length
- modelling thermal, electromagnetic effects

...

$\implies n \approx 10^6 \dots 10^9$



- Differential-algebraic equations in circuit simulation
- Passivity and contractivity
- Model order reduction problem
- Positive real balanced truncation
- Bounded real balanced truncation
- Numerical aspects
- Conclusion

# Circuit equations



Consider a linear DAE system

$$E \dot{x}(t) = A x(t) + B u(t)$$

$$y(t) = C x(t) + D u(t)$$

with

$$E = \begin{bmatrix} A_C C A_C^T & 0 & 0 \\ 0 & \mathcal{L} & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad A = \begin{bmatrix} -A_{\mathcal{R}} \mathcal{R}^{-1} A_{\mathcal{R}}^T & -A_{\mathcal{L}}^T & -A_{\mathcal{V}}^T \\ A_{\mathcal{L}}^T & 0 & 0 \\ A_{\mathcal{V}}^T & 0 & 0 \end{bmatrix}, \quad B = \begin{bmatrix} -A_{\mathcal{I}} & 0 \\ 0 & 0 \\ 0 & -I \end{bmatrix} = C^T,$$

$$u(t) = \begin{bmatrix} j_{\mathcal{I}}(t) \\ v_{\mathcal{V}}(t) \end{bmatrix} \in \mathbb{R}^m, \quad x(t) = \begin{bmatrix} \eta(t) \\ j_{\mathcal{L}}(t) \\ j_{\mathcal{V}}(t) \end{bmatrix} \in \mathbb{R}^n, \quad y(t) = \begin{bmatrix} v_{\mathcal{I}}(t) \\ j_{\mathcal{V}}(t) \end{bmatrix} \in \mathbb{R}^m,$$

$\eta(t)$  – node potentials,

$j_{\mathcal{L}}(t), j_{\mathcal{V}}(t), j_{\mathcal{I}}(t)$  – currents through inductors, voltage and current sources,

$v_{\mathcal{V}}(t), v_{\mathcal{I}}(t)$  – voltages at voltage and current sources,

$A_{\mathcal{R}}, A_C, A_{\mathcal{L}}, A_{\mathcal{V}}, A_{\mathcal{I}}$  – incidence matrices of resistors, capacitors, inductors, voltage and current sources,

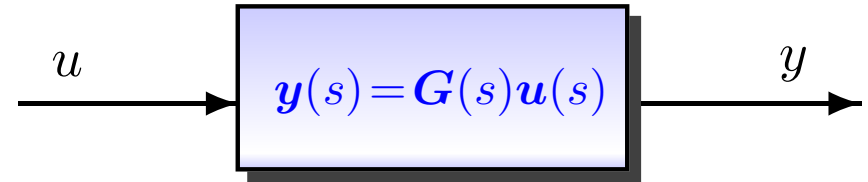
$\mathcal{R}, C, \mathcal{L} > 0$  – resistance, capacitance and inductance matrices.

# Frequency domain representation



Transfer function:

$$G(s) = C(sE - A)^{-1}B + D$$



Weierstrass canonical form:

$$E = T_l \begin{bmatrix} I & 0 \\ 0 & N \end{bmatrix} T_r, \quad A = T_l \begin{bmatrix} J & 0 \\ 0 & I \end{bmatrix} T_r,$$

where  $T_l, T_r$  – nonsingular,  $J$  – Jordan block,

$N$  – nilpotent ( $N^{\nu-1} \neq 0, N^\nu = 0 \rightsquigarrow \nu$  is **index** of  $\lambda E - A$ ).

$$\hookrightarrow G(s) = C(sE - A)^{-1}B + D = G_{sp}(s) + P(s),$$

where  $G_{sp}(s) = C_1(sI - J)^{-1}B_1$  – strictly proper,

$$P(s) = C_2(sN - I)^{-1}B_2 + D = M_0 + sM_1 + \dots + s^{\nu-1}M_{\nu-1}.$$

# Passivity and contractivity



- $G = [E, A, B, C, D]$  is **passive** (  $\langle u, y \rangle_{\mathbb{L}_2} > 0$  )  
 $\iff G(s) = C(sE - A)^{-1}B + D$  is **positive real**
  - $G(s)$  is analytic in  $\mathbb{C}^+$
  - $G(s) + G^T(\bar{s}) \geq 0$  for all  $s \in \mathbb{C}^+$
- $G = [E, A, B, C, D]$  is **contractive** (  $\|y\|_{\mathbb{L}_2} \leq \|u\|_{\mathbb{L}_2}$  )  
 $\iff G(s) = C(sE - A)^{-1}B + D$  is **bounded real**
  - $G(s)$  is analytic in  $\mathbb{C}^+$
  - $I - G(s)G^T(\bar{s}) \geq 0$  for all  $s \in \mathbb{C}^+$
- $G(s)$  is positive real (bounded real) if and only if  
 $\mathcal{M}(G)(s) = (I - G(s))(I + G(s))^{-1}$  is bounded real (positive real).

# Circuit equations



$$E \dot{x}(t) = A x(t) + B u(t)$$
$$y(t) = C x(t) + D u(t)$$

with

$$E = \begin{bmatrix} A_c C A_c^T & 0 & 0 \\ 0 & \mathcal{L} & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad A = \begin{bmatrix} -A_{\mathcal{R}} \mathcal{R}^{-1} A_{\mathcal{R}}^T & -A_{\mathcal{L}}^T & -A_{\mathcal{V}}^T \\ A_{\mathcal{L}}^T & 0 & 0 \\ A_{\mathcal{V}}^T & 0 & 0 \end{bmatrix}, \quad B = \begin{bmatrix} -A_{\mathcal{I}} & 0 \\ 0 & 0 \\ 0 & -I \end{bmatrix} = C^T,$$

$$u(t) = \begin{bmatrix} j_{\mathcal{I}}(t) \\ v_{\mathcal{V}}(t) \end{bmatrix} \in \mathbb{R}^m, \quad x(t) = \begin{bmatrix} \eta(t) \\ j_{\mathcal{L}}(t) \\ j_{\mathcal{V}}(t) \end{bmatrix} \in \mathbb{R}^n, \quad y(t) = \begin{bmatrix} v_{\mathcal{I}}(t) \\ j_{\mathcal{V}}(t) \end{bmatrix} \in \mathbb{R}^m,$$

We have  $E = E^T \geq 0$ ,  $A + A^T \leq 0$ ,  $B = C^T$  and thus

$$\begin{aligned} G(s) + G^T(\bar{s}) &= B^T (sE - A)^{-1} B + B^T (\bar{s}E - A^T)^{-1} B \\ &= B^T (sE - A)^{-1} (2 \operatorname{Re}(s)E - (A + A^T)) (sE - A)^{-*} B \geq 0. \end{aligned}$$

# Passivity via Lur'e systems



- If  $G = [E, A, B, C, D]$  is passive and R-minimal, then there exist matrices  $\mathcal{X} = \mathcal{X}^T \geq 0$ ,  $J_c$ ,  $K_c$  and  $\mathcal{Y} = \mathcal{Y}^T \geq 0$ ,  $J_o$ ,  $K_o$  that satisfy the projected generalized Lur'e systems

$$\begin{aligned}A \mathcal{X} E^T + E \mathcal{X} A^T &= -K_c K_c^T \\ E \mathcal{X} C^T - P_l B &= -K_c J_c^T \\ \mathcal{X} &= P_r \mathcal{X} P_r^T, \quad K_c = P_l K_c \\ M_0 + M_0^T &= J_c J_c^T\end{aligned}$$

$$\begin{aligned}A^T \mathcal{Y} E + E^T \mathcal{Y} A &= -K_o^T K_o \\ B^T \mathcal{Y} E - C P_r &= -J_o^T K_o \\ \mathcal{Y} &= P_l^T \mathcal{Y} P_l, \quad K_o = K_o P_r \\ M_0 + M_0^T &= J_o^T J_o\end{aligned}$$

- If  $M_1 \geq 0$ ,  $M_k = 0$  for  $k \geq 2$  and the generalized Lur'e systems have the solution, then  $G = [E, A, B, C, D]$  is passive.
- $0 \leq \mathcal{X}_{\min} \leq \mathcal{X} \leq \mathcal{X}_{\max}$ ,  $0 \leq \mathcal{Y}_{\min} \leq \mathcal{Y} \leq \mathcal{Y}_{\max}$   
 $\mathcal{X}_{\min}$  is **positive real controllability Gramian**  
 $\mathcal{Y}_{\min}$  is **positive real observability Gramian**

# Contractivity via Lur'e systems



- If  $G = [E, A, B, C, D]$  is contractive and R-minimal, then there exist matrices  $\mathcal{X} = \mathcal{X}^T \geq 0$ ,  $J_c$ ,  $K_c$  and  $\mathcal{Y} = \mathcal{Y}^T \geq 0$ ,  $J_o$ ,  $K_o$  that satisfy the projected generalized Lur'e systems

$$\begin{aligned} A\mathcal{X}E^T + E\mathcal{X}A^T &= -P_l B B^T P_l^T - K_c K_c^T \\ E\mathcal{X}C^T + P_l B M_0^T &= -K_c J_c^T \\ \mathcal{X} &= P_r \mathcal{X} P_r^T, \quad K_c = P_l K_c \\ I - M_0 M_0^T &= J_c J_c^T \end{aligned}$$

$$\begin{aligned} A^T \mathcal{Y} E + E^T \mathcal{Y} A &= -P_r^T C^T C P_r - K_o^T K_o \\ B^T \mathcal{Y} E + M_0^T C P_r &= -J_o^T K_o \\ \mathcal{Y} &= P_l^T \mathcal{Y} P_l, \quad K_o = K_o P_r \\ I - M_0^T M_0 &= J_o^T J_o \end{aligned}$$

- If  $M_k = 0$  for  $k \geq 1$  and the generalized Lur'e systems have the solution, then  $G = [E, A, B, C, D]$  is contractive.
- $0 \leq \mathcal{X}_{\min} \leq \mathcal{X} \leq \mathcal{X}_{\max}, \quad 0 \leq \mathcal{Y}_{\min} \leq \mathcal{Y} \leq \mathcal{Y}_{\max}$   
 $\mathcal{X}_{\min}$  is **bounded real controllability Gramian**  
 $\mathcal{Y}_{\min}$  is **bounded real observability Gramian**

# BR Gramians: Physical Meaning



Energy that is put into a contractive system:

$$E_{br}(u) := \int_{-\infty}^{\infty} \|u(\tau)\|^2 - \|y(\tau)\|^2 d\tau$$

$$x_0^T \mathcal{X}_{\min}^+ x_0 = \inf \left\{ \int_{-\infty}^0 \|u(\tau)\|^2 - \|y(\tau)\|^2 d\tau : u \in C(\mathbb{R}^-, \mathbb{R}^m) \cap L_2(\mathbb{R}^-, \mathbb{R}^m) \right. \\ \left. \text{and } u \text{ controls to } x(0) = x_0 \right\},$$

*Required supply:* Minimum amount of energy that must be provided by the environment to the system in order to control the system to state  $x(0) = x_0$  over any possible trajectory.

$$x_0^T E^T \mathcal{Y}_{\min} E x_0 = \sup \left\{ \int_0^{\infty} \|u(\tau)\|^2 - \|y(\tau)\|^2 d\tau : u \in C(\mathbb{R}^+, \mathbb{R}^m) \cap L_2(\mathbb{R}^+, \mathbb{R}^m) \right. \\ \left. \text{and } u \text{ is consistent with } x(0) = x_0 \right\},$$

*Available storage energy:* Maximum energy that can be extracted from the system over any possible trajectory of the state from an initial state  $x(0) = x_0$ .

# Model reduction problem



**Given** a descriptor system

$$E \dot{x}(t) = A x(t) + B u(t)$$

$$y(t) = C x(t) + D u(t)$$

with  $E, A \in \mathbb{R}^{n,n}$ ,  $B \in \mathbb{R}^{n,m}$ ,  
 $C \in \mathbb{R}^{p,n}$ ,  $D \in \mathbb{R}^{p,m}$ ,  $n \gg m, p$ ,

**find** a reduced-order system

$$\tilde{E} \dot{\tilde{x}}(t) = \tilde{A} \tilde{x}(t) + \tilde{B} u(t)$$

$$\tilde{y}(t) = \tilde{C} \tilde{x}(t) + \tilde{D} u(t)$$

with  $\tilde{E}, \tilde{A} \in \mathbb{R}^{\ell,\ell}$ ,  $\tilde{B} \in \mathbb{R}^{\ell,m}$ ,  
 $\tilde{C} \in \mathbb{R}^{p,\ell}$ ,  $\tilde{D} \in \mathbb{R}^{p,m}$ ,  $\ell \ll n$ .

**Given**

$$G(s) = C(sE - A)^{-1}B + D,$$

**find**

$$\tilde{G}(s) = \tilde{C}(s\tilde{E} - \tilde{A})^{-1}\tilde{B} + \tilde{D}$$

s.t.  $\|\tilde{G} - G\| \rightarrow \min.$

- preserve system properties ( passivity, contractivity, ... )
- small approximation error (  $\|\tilde{y} - y\|$  or  $\|\tilde{G} - G\|$  )
- numerically stable and efficient methods



- **Krylov subspace methods** ( moment matching )
  - stability and passivity are in general not guaranteed
    - SyPVL preserves passivity for RC, RL, LC circuits [ Freund et al.'96,'97 ]
    - PRIMA preserves passivity for RLC circuits [ Odabasioglu et al.'96,'97 ]
    - SPRIM preserves passivity / reciprocity for RLC circuits [ Freund'04.'05 ]
    - Laguerre-SVD preserves passivity for RLC circuits [ Knockaert et al.'00 ]
    - Positive real interpolation preserves passivity [ Antoulas'05, Sorensen'05 ]
  - no computable error bound
  - choice of interpolation points / spectral zeros
- **Balancing-related model reduction methods**
  - stability and passivity are preserved
  - there exist global computable error bounds
  - solution of Lyapunov / Riccati / Lur'e matrix equations

# PR and BR balanced truncation



•  $G = [E, A, B, C, D]$  is **positive / bounded real balanced**,

if  $\mathcal{X}_{\min} = \mathcal{Y}_{\min} = \begin{bmatrix} \Pi & \\ & 0 \end{bmatrix}$  with  $\Pi = \text{diag}(\pi_1, \dots, \pi_{n_f})$ .

•  $\pi_j = \sqrt{\lambda_j(\mathcal{X}_{\min} E^T \mathcal{Y}_{\min} E)}$  are characteristic values

**Idea:** **balance** the system, i.e., find an equivalence transformation

$$[\hat{E}, \hat{A}, \hat{B}, \hat{C}, \hat{D}] = [W_b E T_b, W_b A T_b, W_b B, C T_b, D]$$

such that  $\hat{\mathcal{X}}_{\min} = \hat{\mathcal{Y}}_{\min} = \text{diag}(\pi_1, \dots, \pi_{n_f}, 0, \dots, 0)$  and

**truncate** the states corresponding to small  $\pi_j$ .

# PR / BR balanced truncation method



Given a passive / contractive system  $\mathbf{G} = [E, A, B, C, D]$  with the proper transfer function  $\mathbf{G}(s) = C(sE - A)^{-1}B + D$ .

1. Compute  $M_0 = D + C(s_0E - A)^{-1}(I - P_l)B$ ,  $s_0 \notin \text{Sp}(E, A)$ ;
2. Compute  $Z_r, Z_l \in R^{n, n_\infty}$  with  $\text{Im } Z_r = \ker P_r$ ,  $\text{Im } Z_l = \ker P_l^T$ ;
3. Compute  $\mathcal{X}_{\min} = RR^T$ ,  $\mathcal{Y}_{\min} = LL^T$  (= solve the Lur'e systems);
4. Compute the SVD  $L^T E R = [U_1, U_2] \begin{bmatrix} \Pi_1 & \\ & \Pi_2 \end{bmatrix} [V_1, V_2]^T$ ;
5. Compute  $\tilde{\mathbf{G}} = [W^T E T, W^T A T, W^T B, C T, M_0]$  with  
 $W = [L U_1 \Pi_1^{-1/2}, Z_l]$  and  $T = [R V_1 \Pi_1^{-1/2}, Z_r]$ .



- Positive real balanced truncation

- $\tilde{\mathbf{G}} = [\tilde{\mathbf{E}}, \tilde{\mathbf{A}}, \tilde{\mathbf{B}}, \tilde{\mathbf{C}}, \tilde{\mathbf{D}}]$  is passive, positive real balanced

- **Error bound:**

$$\begin{aligned} \|\tilde{\mathbf{G}} - \mathbf{G}\|_{\infty} &:= \sup_{\omega \in \mathbb{R}} \|\tilde{\mathbf{G}}(i\omega) - \mathbf{G}(i\omega)\| \\ &\leq 2 \|M_0 + M_0^T\|^2 \|\mathbf{G} + M_0^T\|_{\infty} \|\tilde{\mathbf{G}} + M_0^T\|_{\infty} \sum_{j=\ell_f+1}^{n_f} \pi_j \end{aligned}$$

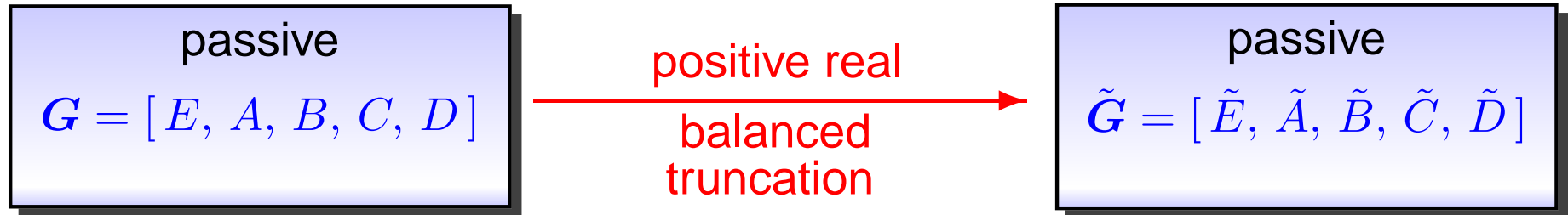
- Bounded real balanced truncation

- $\tilde{\mathbf{G}} = [\tilde{\mathbf{E}}, \tilde{\mathbf{A}}, \tilde{\mathbf{B}}, \tilde{\mathbf{C}}, \tilde{\mathbf{D}}]$  is contractive, bounded real balanced

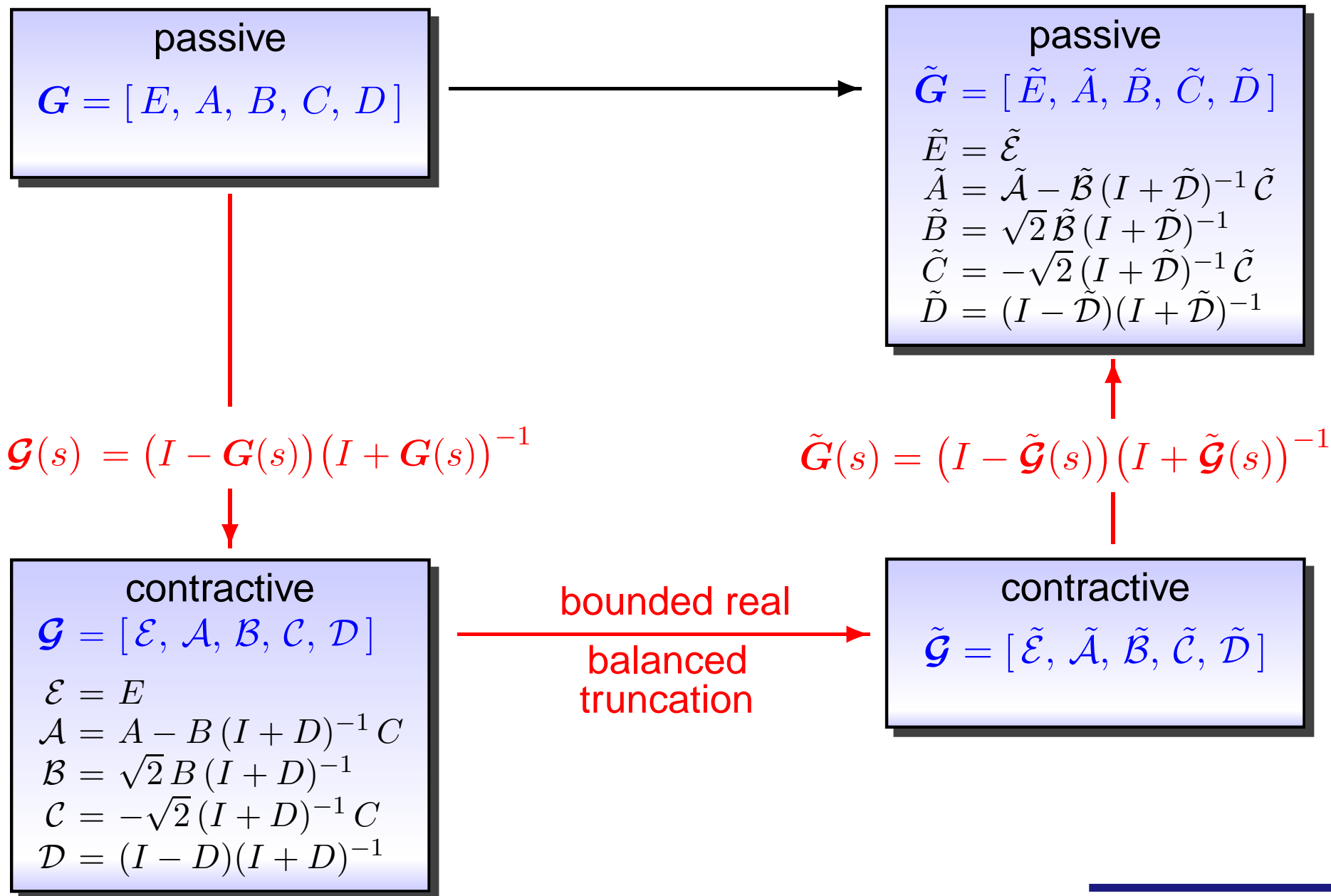
- **Error bound:**

$$\|\tilde{\mathbf{G}} - \mathbf{G}\|_{\infty} \leq 2 \sum_{j=\ell_f+1}^{n_f} \pi_j$$

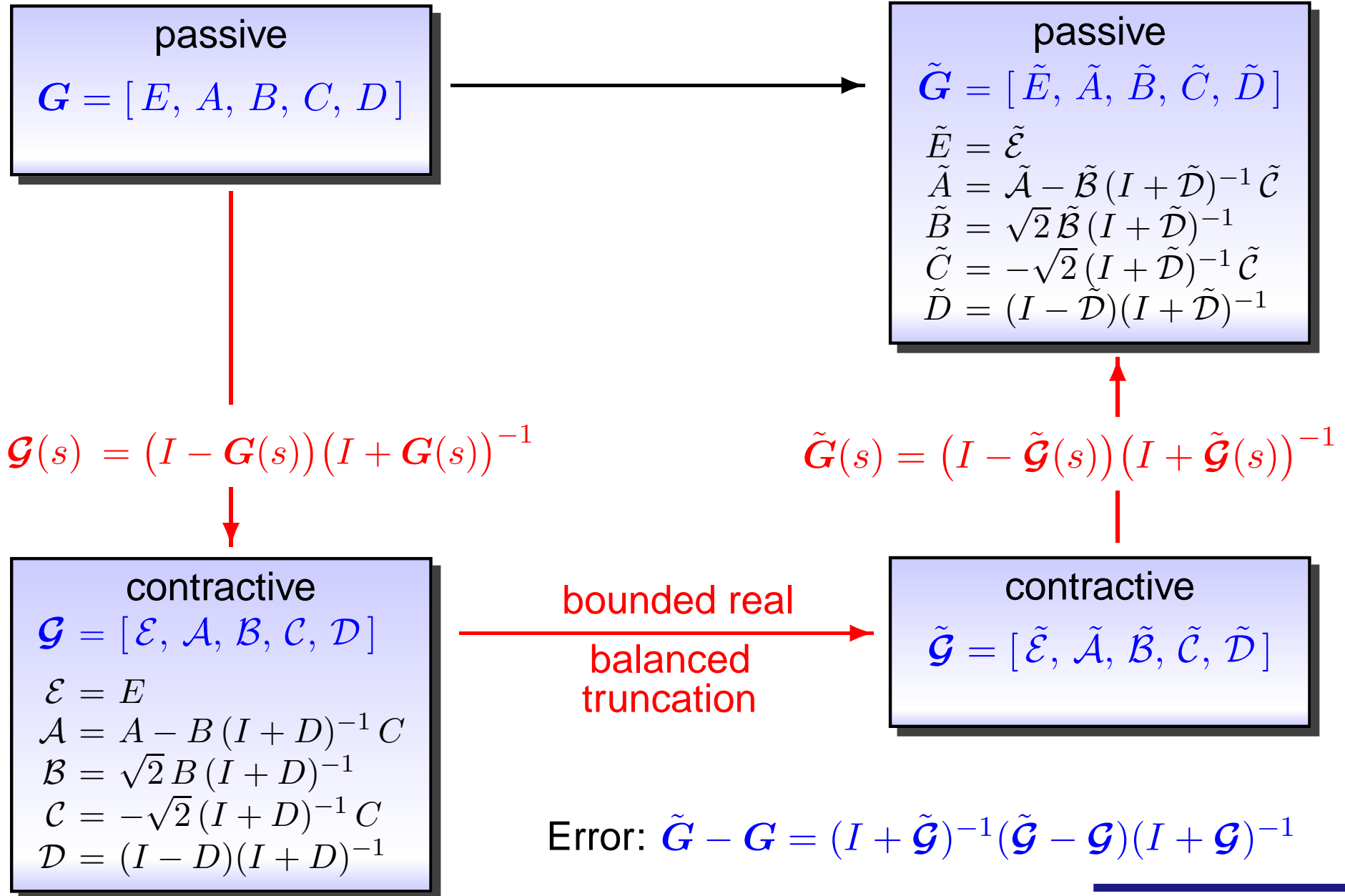
# Passivity-preserving model reduction



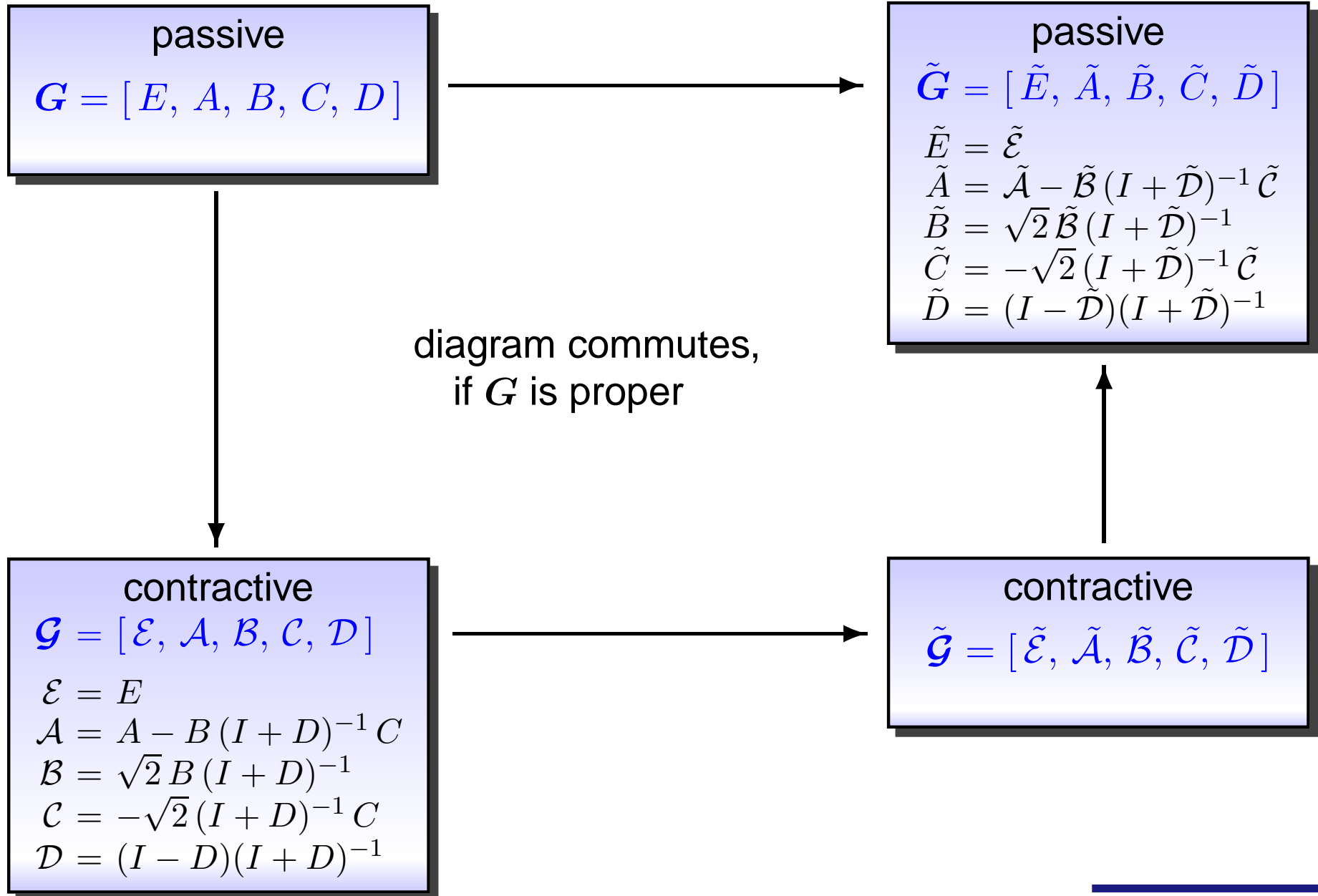
# Passivity-preserving model reduction



# Passivity-preserving model reduction



# Passivity-preserving model reduction



# BR Gramians of Moebius Transformed System



Energy that is put into a passive system:

$$E_{br}(u) := \int_{-\infty}^{\infty} u(\tau)^T y(\tau) d\tau$$

$$x_0^T \mathcal{X}_{\min}^+ x_0 = 2 \inf \left\{ \int_{-\infty}^0 u(\tau)^T y(\tau) d\tau : u \in C^1(\mathbb{R}^-, \mathbb{R}^m) \cap L_2(\mathbb{R}^-, \mathbb{R}^m) \right. \\ \left. \text{and } u \text{ controls to } x(0) = x_0 \right\},$$

*Required supply:* Minimum amount of energy that must be provided by the environment to the system in order to control the system to state  $x(0) = x_0$  over any possible trajectory.

$$x_0^T E^T \mathcal{Y}_{\min} E x_0 = 2 \sup \left\{ \int_0^{\infty} u(\tau)^T y(\tau) d\tau : u \in C^1(\mathbb{R}^+, \mathbb{R}^m) \cap L_2(\mathbb{R}^+, \mathbb{R}^m) \right. \\ \left. \text{and } u \text{ is consistent with } x(0) = x_0 \right\},$$

*Available storage energy:* Maximum energy that can be extracted from the system over any possible trajectory of the state from an initial state  $x(0) = x_0$ .



- For  $S_i = \text{diag}(I_{n_x}, -I_{n_L}, -I_{n_v}) = S_i^T$  and  $S_e = \text{diag}(I_{n_I}, -I_{n_v}) = S_e^T$ , we have

$$E^T = S_i E S_i, \quad A^T = S_i A S_i \quad \text{and} \quad B^T = S_e C S_i$$

$$\hookrightarrow P_l = S_i P_r^T S_i \quad \text{and} \quad \mathcal{X}_{\min} = S_i \mathcal{Y}_{\min} S_i^T = S_i L L^T S_i^T = R R^T$$

$$\hookrightarrow L^T E R = L^T E S_i L \quad \text{is symmetric}$$

$$\hookrightarrow \text{compute the eigenvalue decomposition } L^T E S_i L = U \Lambda U^T \text{ (instead of the SVD)}$$

- Transfer function satisfies  $G(s)S_e = S_e G(s)^T$  (reciprocity)

This property is preserved by the reduced order model,

$$\text{i.e. } \tilde{G}(s)S_e = S_e \tilde{G}(s)^T.$$

# Numerical aspects: Projectors for Circuits

- compute  $P_r$  using the block structure of  $\mathbf{G} = [E, A, B, C, D]$

$$\text{with } E = \begin{bmatrix} A_c C A_c^T & 0 & 0 \\ 0 & \mathcal{L} & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad A = \begin{bmatrix} -A_{\mathcal{R}} \mathcal{R}^{-1} A_{\mathcal{R}}^T & -A_{\mathcal{L}}^T & -A_{\mathcal{V}}^T \\ A_{\mathcal{L}}^T & 0 & 0 \\ A_{\mathcal{V}}^T & 0 & 0 \end{bmatrix}$$

$\hookrightarrow P_r$  is available only for RC circuits or index 1 circuits

- compute  $P_r$  using the block structure of the Moebius-transformed system  $\mathbf{G} = [\mathcal{E}, \mathcal{A}, \mathcal{B}, \mathcal{C}, \mathcal{D}]$  with

$$\mathcal{E} = \begin{bmatrix} A_c C A_c^T & 0 & 0 \\ 0 & \mathcal{L} & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad \mathcal{A} = \begin{bmatrix} -A_{\mathcal{R}} \mathcal{R}^{-1} A_{\mathcal{R}}^T - A_{\mathcal{I}} A_{\mathcal{I}}^T & -A_{\mathcal{L}}^T & -A_{\mathcal{V}}^T \\ A_{\mathcal{L}}^T & 0 & 0 \\ A_{\mathcal{V}}^T & 0 & -I \end{bmatrix}$$

$\hookrightarrow \lambda \mathcal{E} - \mathcal{A}$  is of index at most 2

$\hookrightarrow P_r$  can be constructed in explicit form using the canonical projectors technique from [März'96]

# Numerical aspects: Projectors for Circuits



If the circuit does not contain inductive cutsets, the projector  $P_r$  for the Moebius-transformed system has the form

$$P_r = \begin{bmatrix} I - H^{-1}Q_c^T Z & -H^{-1}Q_c^T A_L & 0 \\ 0 & I & 0 \\ A_v^T(I - H^{-1}Q_c^T Z) & -A_v^T H^{-1}Q_c^T A_L & 0 \end{bmatrix},$$

where

$$Z = A_{\mathcal{R}} \mathcal{R}^{-1} A_{\mathcal{R}}^T + A_v A_v^T + A_I A_I^T,$$
$$H = (I - Q_c)^T (I - Q_c) + Q_c^T Z Q_c,$$

and  $Q_c$  is a projector with  $\text{Im } Q_c = \ker A_c$ .



- If  $\hat{D} = M_0 + M_0^T$  is nonsingular, then the positive real Lur'e system is equivalent to the projected Riccati equation

$$A^T \mathcal{Y} E + E^T \mathcal{Y} A + (B^T \mathcal{Y} E - C P_r)^T \hat{D}^{-1} (B^T \mathcal{Y} E - C P_r) = 0$$
$$\mathcal{Y} = P_l^T \mathcal{Y} P_l$$

- If  $\hat{D} = I - M_0^T M_0$  is nonsingular, then the bounded real Lur'e system is equivalent to the projected Riccati equation

$$A^T \mathcal{Y} E + E^T \mathcal{Y} A + P_r^T C^T C P_r + (B^T \mathcal{Y} E + M_0^T C P_r)^T \hat{D}^{-1} (B^T \mathcal{Y} E + M_0^T C P_r) = 0$$
$$\mathcal{Y} = P_l^T \mathcal{Y} P_l$$

# Numerical aspects: Lur'e systems



Consider an extended Hamiltonian pencil

$$\lambda \mathcal{M} - \mathcal{N} = \lambda \begin{bmatrix} E & 0 & 0 \\ 0 & E^T & 0 \\ 0 & 0 & 0 \end{bmatrix} - \begin{bmatrix} A & 0 & P_l B \\ -P_r^T F P_r & -A^T & -P_r^T \hat{C}^T \\ \hat{C} P_r & B^T P_l^T & \hat{D} \end{bmatrix},$$

where  $F = 0$ ,  $\hat{C} = -C$ ,  $\hat{D} = M_0 + M_0^T$  in the positive real case  
and  $F = C^T C$ ,  $\hat{C} = M_0^T C$ ,  $\hat{D} = I - M_0^T M_0$  in the bounded real case.

If

$$\mathcal{M} \begin{bmatrix} Z_1 \\ Z_2 \\ Z_3 \end{bmatrix} \Lambda_- = \mathcal{N} \begin{bmatrix} Z_1 \\ Z_2 \\ Z_3 \end{bmatrix}, \quad \text{Sp}(\Lambda_-) \subset \mathbb{C}_-,$$

where  $Z_1 \in \mathbb{R}^{n, n_f}$  has full column rank, then  $\mathcal{Y}_{\min} = Z_2 (E Z_1)^-$ .

- Often,  $\mathcal{Y}_{\min}$  has low numerical rank
  - ↪ compute a low-rank factor of  $\mathcal{Y}_{\min}$ , i.e.,  $\mathcal{Y}_{\min} \approx \tilde{L} \tilde{L}^T$ ,  $\tilde{L} \in \mathbb{R}^{n, r}$
  - ↪ compute the eigenvalue decomposition of  $\tilde{L}^T E S \tilde{L} \in \mathbb{R}^{r, r}$

# Numerical aspects: Riccati equations



Consider the projected generalized Riccati equation

$$A^T \mathcal{Y} E + E^T \mathcal{Y} A + P_r^T F P_r + (B^T \mathcal{Y} E + \hat{C} P_r)^T \hat{D}^{-1} (B^T \mathcal{Y} E + \hat{C} P_r) = 0,$$
$$\mathcal{Y} = P_l^T \mathcal{Y} P_l.$$

## Generalized Newton's method:

For  $k = 0, 1, 2, \dots$

1. Compute  $A_k = A - P_l B \hat{D}^{-1} B^T \mathcal{Y}_k E P_r$  and

$$G_k = A^T \mathcal{Y}_k E + E^T \mathcal{Y}_k A + P_r^T F P_r + (B^T \mathcal{Y}_k E + \hat{C} P_r)^T \hat{D}^{-1} (B^T \mathcal{Y}_k E + \hat{C} P_r).$$

2. Solve the projected generalized Lyapunov equation

$$A_k^T \mathcal{N}_k E + E^T \mathcal{N}_k A_k = -P_r^T G_k P_r, \quad \mathcal{N}_k = P_l^T \mathcal{N}_k P_l.$$

3. Update  $\mathcal{Y}_{k+1} = \mathcal{Y}_k + \mathcal{N}_k$ .

Properties:

- $\lambda E - A_k$  is stable and  $\mathcal{Y}_k = P_l^T \mathcal{Y}_k P_l$
- $\lim_{k \rightarrow \infty} G_k = 0$  and  $\lim_{k \rightarrow \infty} \mathcal{Y}_k = \mathcal{Y}$
- solve the projected Lyapunov equation via the gen. ADI method [Stykel'04] or the gen. sign function method [Stykel'07]



- Passivity-preserving model reduction of circuit equations
  - positive real balanced truncation
  - bounded real balanced truncation of the Moebius-transformed system
- Projectors  $P_r$  and  $P_l$  are required
  - ↔ exploit the structure of  $E$  and  $A$
  - ↔ exploit the circuit topology ( work in progress )
- Implementation of Lur'e system solvers is in progress
  - Newton method for the projected Riccati equations
  - computing the stable subspaces of  $\lambda\mathcal{M} - \mathcal{N}$ 
    - ↔ exploit the structure of  $\mathcal{M}$  and  $\mathcal{N}$
- Interpretation of passive reduced order model as an electrical circuit
  - ↔ circuit synthesis ( work in progress )