

SQP methods for incremental plasticity

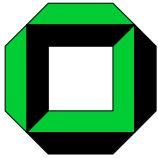
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From Elasticity to Plasticity

Elasticity describes (reversible) deformations of a body under loading.

The elastic deformations are determined by minimizing the elastic energy.

The minimizer is characterized by an *equilibrium equation* for the stress and a *constitutive equation* for the relation of deformation and stress.

In linear elasticity, the stress is given by $\boldsymbol{\sigma} = \mathbb{C} : \boldsymbol{\varepsilon}(\mathbf{u})$ depending on the (linearized) strain $\boldsymbol{\varepsilon}(\mathbf{u}) = \text{sym}(D\mathbf{u})$, where \mathbf{u} is the displacement vector.

The Hookian tensor defined by $\mathbb{C} : \boldsymbol{\varepsilon} = 2\mu_S \boldsymbol{\varepsilon} + \lambda_S \text{trace}[\boldsymbol{\varepsilon}] \mathbf{I}$ with Lamé constants $\lambda_S, \mu_S > 0$.

Plasticity describes the failure of the elastic relations leading to irreversible deformations of a body under loading.

Classical plasticity models limit extreme stress values at every material point.

A simple plasticity model is obtained by a convex yield function $\phi(\boldsymbol{\sigma}) = |\text{dev}(\boldsymbol{\sigma})| - K_0$ determining the convex set of admissible stresses $\mathbf{K} = \{\boldsymbol{\sigma} \in \text{Sym}(d) : \phi(\boldsymbol{\sigma}) \leq 0\}$.

Here, the deviator $\text{dev}(\boldsymbol{\sigma}) = \boldsymbol{\sigma} - \frac{1}{d} \text{trace}(\boldsymbol{\sigma}) \mathbf{I}$ denotes the shear part of the stress.

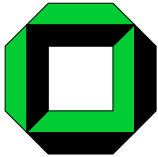
Plasticity fits into the framework of convex analysis and convex programming.

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Infinitesimal perfect plasticity: Data

Let $\Omega \subset \mathbb{R}^d$ ($d = 2, 3$) be the reference configuration, and let $\Gamma_D \cup \Gamma_N = \partial\Omega$ be a decomposition of the boundary. We fix a time interval $[0, T]$.

The problem depends on the following data: a prescribed displacement vector

$$\mathbf{u}_D: \Gamma_D \times [0, T] \longrightarrow \mathbb{R}^d$$

for the essential boundary conditions on Γ_D , and a load functional

$$\ell(t, \mathbf{v}) = \int_{\Omega} \mathbf{b}(t) \cdot \mathbf{v} d\mathbf{x} + \int_{\Gamma_N} \mathbf{t}_N(t) \cdot \mathbf{v} da$$

depending on body force densities and traction force densities

$$\mathbf{b}: \Omega \times [0, T] \longrightarrow \mathbb{R}^d, \quad \mathbf{t}_N: \Gamma_N \times [0, T] \longrightarrow \mathbb{R}^d .$$

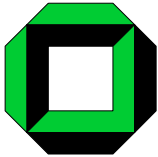
We start with the initial state $\mathbf{u}_D(0) = \mathbf{0}$, $\mathbf{b}(0) = \mathbf{0}$, $\mathbf{t}_N(0) = \mathbf{0}$.

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The equations of infinitesimal plasticity

We want to determine

displacements	$\mathbf{u}: \bar{\Omega} \times [0, T] \longrightarrow \mathbb{R}^d,$
stresses	$\boldsymbol{\sigma}: \Omega \times [0, T] \longrightarrow \text{Sym}(d),$
plastic strains	$\boldsymbol{\varepsilon}_p: \Omega \times [0, T] \longrightarrow \text{Sym}(d),$
a plastic multiplier	$\lambda: \Omega \times [0, T] \longrightarrow \mathbb{R}$

satisfying the essential boundary conditions

$$\mathbf{u}(\mathbf{x}, t) = \mathbf{u}_D(\mathbf{x}, t), \quad (\mathbf{x}, t) \in \Gamma_D \times [0, T],$$

the constitutive relation

$$\boldsymbol{\sigma}(\mathbf{x}, t) = \mathbf{C} : \left(\boldsymbol{\varepsilon}(\mathbf{u})(\mathbf{x}, t) - \boldsymbol{\varepsilon}_p(\mathbf{x}, t) \right), \quad (\mathbf{x}, t) \in \Omega \times [0, T],$$

the **equilibrium equations**

$$\begin{aligned} -\text{div } \boldsymbol{\sigma}(\mathbf{x}, t) &= \mathbf{b}(\mathbf{x}, t), & (\mathbf{x}, t) \in \Omega \times [0, T], \\ \boldsymbol{\sigma}(\mathbf{x}, t) \cdot \mathbf{n}(\mathbf{x}) &= \mathbf{t}_N(\mathbf{x}, t), & (\mathbf{x}, t) \in \Gamma_N \times [0, T] \end{aligned}$$

(where $\mathbf{n}(\mathbf{x})$ denotes the outer unit normal vector), the **flow rule**

$$\frac{d}{dt} \boldsymbol{\varepsilon}_p(\mathbf{x}, t) = \lambda(\mathbf{x}, t) D\phi(\boldsymbol{\sigma}(\mathbf{x}, t)), \quad (\mathbf{x}, t) \in \Omega \times [0, T],$$

and the **complementary conditions (Kuhn-Tucker)**

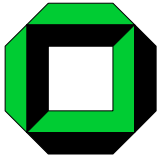
$$\lambda(\mathbf{x}, t) \phi(\boldsymbol{\sigma}(\mathbf{x}, t)) = 0, \quad \lambda(\mathbf{x}, t) \geq 0, \quad \phi(\boldsymbol{\sigma}(\mathbf{x}, t)) \leq 0, \quad (\mathbf{x}, t) \in \Omega \times [0, T].$$

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Discretization in space

Let $\mathbf{V} \subset C(\bar{\Omega}, \mathbb{R}^d)$ be a finite element space spanned by nodal basis functions, and let

$$\mathbf{V}(\mathbf{u}_D) = \{\mathbf{v} \in \mathbf{V} : \mathbf{v}(\mathbf{x}) = \mathbf{u}_D(\mathbf{x}) \text{ for } \mathbf{x} \in D\},$$

where $D \subset \Gamma_D$ is the set of all nodal points on Γ_D .

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Let $\Xi \subset \Omega$ be quadrature points and let ω_ξ be corresponding quadrature weights such that

$$\int_{\Omega} \mathbf{v} \cdot \mathbf{w} d\mathbf{x} = \sum_{\xi \in \Xi} \omega_\xi \mathbf{v}(\xi) \cdot \mathbf{w}(\xi), \quad \mathbf{v}, \mathbf{w} \in \mathbf{V}.$$

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We set $\Lambda = \{\mu : \Xi \rightarrow \mathbb{R}\}$ and $\Sigma = \{\tau : \Xi \rightarrow \text{Sym}(d)\}$.

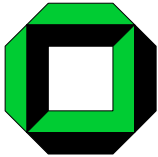
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For given $\mathbf{u} \in \mathbf{V}$ this defines $\sigma = \mathbf{C} : \varepsilon(\mathbf{u}) \in \Sigma$.

In our notation the integral is used also for the finite sums

$$\int_{\Omega} \sigma : \varepsilon d\mathbf{x} := \sum_{\xi \in \Xi_h} \omega_\xi \sigma(\xi) : \varepsilon(\xi), \quad \sigma, \varepsilon \in \Sigma.$$

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Discretization in time

The model of incremental infinitesimal plasticity is obtained by a decomposition

$$0 = t_0 < t_1 < \dots < t_N = T$$

of the time interval and the backward Euler scheme: given $\varepsilon_p^0 = \mathbf{0}$ at $t_0 = 0$, compute for $n = 1, 2, 3, \dots$ the displacement $\mathbf{u}^n \in \mathbf{V}(\mathbf{u}_D^n)$ satisfying the essential boundary conditions, the stress $\boldsymbol{\sigma}^n \in \Sigma$, the plastic strain $\varepsilon_p^n \in \Sigma$, and the plastic multiplier $\lambda^n \in \Lambda$ satisfying the constitutive relation

$$\boldsymbol{\sigma}^n(\xi) = \mathbf{C} : \left(\boldsymbol{\varepsilon}(\mathbf{u}^n)(\xi) - \varepsilon_p^n(\xi) \right), \quad \xi \in \Xi,$$

the **equilibrium equation**

$$\int_{\Omega} \boldsymbol{\sigma}^n : \boldsymbol{\varepsilon}(\mathbf{v}) \, d\mathbf{x} = \ell(t_n, \mathbf{v}), \quad \mathbf{v} \in \mathbf{V}(\mathbf{0}),$$

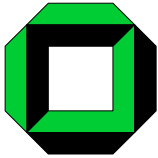
the **flow rule**

$$\frac{1}{t_n - t_{n-1}} \left(\varepsilon_p^n(\xi) - \varepsilon_p^{n-1}(\xi) \right) = \lambda^n(\xi) D\phi(\boldsymbol{\sigma}^n(\xi)), \quad \xi \in \Xi$$

and the **complementary conditions (Kuhn-Tucker)**

$$\lambda^n(\xi) \phi(\boldsymbol{\sigma}^n(\xi)) = 0, \quad \lambda^n(\xi) \geq 0, \quad \phi(\boldsymbol{\sigma}^n(\xi)) \leq 0, \quad \xi \in \Xi.$$

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Incremental plasticity

Since the problem is rate-independent, rescaling of the time parameter does not affect the model. Thus, we define

$$\gamma^n = 2\mu_S(t_n - t_{n-1})\lambda^n \in \Lambda ,$$

i. e., the discretized flow rule has the form

$$\varepsilon_p^n(\xi) = \varepsilon_p^{n-1}(\xi) + \frac{\gamma^n(\xi)}{2\mu_S} D\phi(\sigma^n(\xi)) , \quad \xi \in \Xi .$$

Now, we can state the fully discrete elasto-plastic problem:

for given $\varepsilon_p^{n-1} \in \Sigma$ find $\sigma^n \in \Sigma$, $\mathbf{u}^n \in \mathbf{V}(\mathbf{u}_D^n)$, and $\gamma^n \in \Lambda$ such that holds:

the flow rule, the complementary condition (Kuhn-Tucker), and the equilibrium equation

$$(FR_n) \quad \sigma^n(\xi) = \mathbf{C} : (\varepsilon(\mathbf{u}^n(\xi)) - \varepsilon_p^{n-1}(\xi)) - \gamma^n(\xi) D\phi(\sigma^n(\xi)) , \quad \xi \in \Xi ,$$

$$(KT_n) \quad \phi(\sigma^n(\xi)) \leq 0, \quad \gamma^n(\xi) \phi(\sigma^n(\xi)) = 0, \quad \gamma^n(\xi) \geq 0, \quad \xi \in \Xi ,$$

$$(EE_n) \quad \int_{\Omega} \sigma^n : \varepsilon(\mathbf{v}) d\mathbf{x} = \ell^n[\mathbf{v}] , \quad \mathbf{v} \in \mathbf{V}(\mathbf{0}) .$$

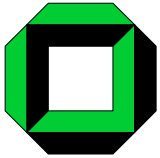
Then, for the next time step ε_p^n is determined by the discretized flow rule.

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Projection onto the set of admissible stresses

Let $P_{\mathbf{K}}: \text{Sym}(d) \rightarrow \mathbf{K}$ be the projection onto the convex set of admissible stresses.

Lemma For given $\theta \in \text{Sym}(d)$ the projection $\sigma = P_{\mathbf{K}}(\theta) \in \mathbf{K}$ is uniquely determined by the solution $(\sigma, \gamma) \in \text{Sym}(d) \times \mathbb{R}$ of the KKT-system

$$\begin{aligned} \mathbf{0} &= \sigma - \theta + \gamma D\phi(\sigma), \\ 0 &\geq \phi(\sigma), \quad \gamma\phi(\sigma) = 0, \quad \gamma \geq 0. \end{aligned}$$

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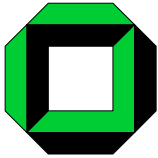
Starting with $\sigma^0 = \theta$ and $\gamma^0 = 0$, the projection can be computed by the Newton iteration

$$\begin{aligned} \mathbf{0} &= \sigma^{m-1} - \theta + \gamma^{m-1} D\phi(\sigma^{m-1}) + \left(\Delta\sigma^m + \gamma^{m-1} D^2\phi(\sigma^{m-1}) : \Delta\sigma^m + \Delta\gamma^m D\phi(\sigma^{m-1}) \right) \\ 0 &= \phi(\sigma^{m-1}) + D\phi(\sigma^{m-1}) : \Delta\sigma^m \end{aligned}$$

and $\sigma^m = \sigma^{m-1} + \Delta\sigma^m$, $\gamma^m = \gamma^{m-1} + \Delta\gamma^m$.

Every Newton step is again a projection: we have $\sigma^m = P^m(\theta^m)$, where $P^m: \text{Sym}(d) \rightarrow \mathbf{K}^m$ be the linearized orthogonal projection onto the halfspace

$$\mathbf{K}^m = \{ \tau \in \text{Sym}(d) : \phi(\sigma^{m-1}) + D\phi(\sigma^{m-1}) : (\tau - \sigma^{m-1}) \} \supset \mathbf{K} .$$



I. The projection method — a semismooth Newton iteration

Lemma The system of incremental plasticity is equivalent to the following nonlinear variational problem: for given ε_p^{n-1} find $\mathbf{u}^n \in \mathbf{V}(\mathbf{u}_D^n)$ such that

$$\int_{\Omega} P_{\mathbf{K}}(\mathbf{C} : (\varepsilon(\mathbf{u}^n) - \varepsilon_p^{n-1})) : \varepsilon(\mathbf{v}) d\mathbf{x} = \ell^n[\mathbf{v}], \quad \mathbf{v} \in \mathbf{V}(\mathbf{0}) .$$

The standard method in computational plasticity is a semismooth Newton iteration

$$0 \in F^n(\mathbf{u}^{n,k-1}) + \partial F^n(\mathbf{u}^{n,k-1}) \Delta \mathbf{u}^{n,k}, \quad \mathbf{u}^{n,k} = \mathbf{u}^{n,k-1} + s^{n,k} \Delta \mathbf{u}^{n,k}, \quad k = 1, 2, 3, \dots$$

where $F^n(\mathbf{u})[\mathbf{v}] = \int_{\Omega} P_{\mathbf{K}}(\mathbf{C} : (\varepsilon(\mathbf{u}) - \varepsilon_p^{n-1})) : \varepsilon(\mathbf{v}) d\mathbf{x} - \ell^n[\mathbf{v}]$ and $s^{n,k} \in (0, 1]$.

Lemma For $\phi(\sigma) = |\text{dev}(\sigma)| - K_0$ we have $P_{\mathbf{K}}(\theta) = \theta - m(|\text{dev}(\theta)| - K_0) \frac{\text{dev}(\theta)}{|\text{dev}(\theta)|}$ and

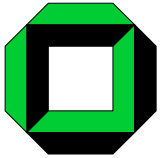
$$\begin{aligned} \partial P_{\mathbf{K}}(\theta) = & \text{id} - \partial m(|\text{dev}(\theta)| - K_0) \frac{\text{dev}(\theta)}{|\text{dev}(\theta)|} \otimes \frac{\text{dev}(\theta)}{|\text{dev}(\theta)|} \\ & - \frac{m(|\text{dev}(\theta)| - K_0)}{|\text{dev}(\theta)|} \left(\left(\text{id} - \frac{1}{d} \mathbf{I} \otimes \mathbf{I} \right) - \frac{\text{dev}(\theta)}{|\text{dev}(\theta)|} \otimes \frac{\text{dev}(\theta)}{|\text{dev}(\theta)|} \right), \end{aligned}$$

with $m(s) = \max\{0, s\}$ and $\partial m(s) = \{1\}$ for $s > 0$, $\partial m(0) = [0, 1]$, $\partial m(s) = \{0\}$ for $s < 0$.

Choosing the consistent tangent $\mathbf{C}^{n,k} \in \partial P_{\mathbf{K}}(\mathbf{C} : (\varepsilon(\mathbf{u}^{n,k-1}) - \varepsilon_p^{n-1})) \mathbf{C}$ gives

$$\int_{\Omega} \varepsilon(\Delta \mathbf{u}^{n,k}) : \mathbf{C}^{n,k} : \varepsilon(\mathbf{v}) d\mathbf{x} = -F^n(\mathbf{u}^{n,k-1})[\mathbf{v}] .$$

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I. The projection method

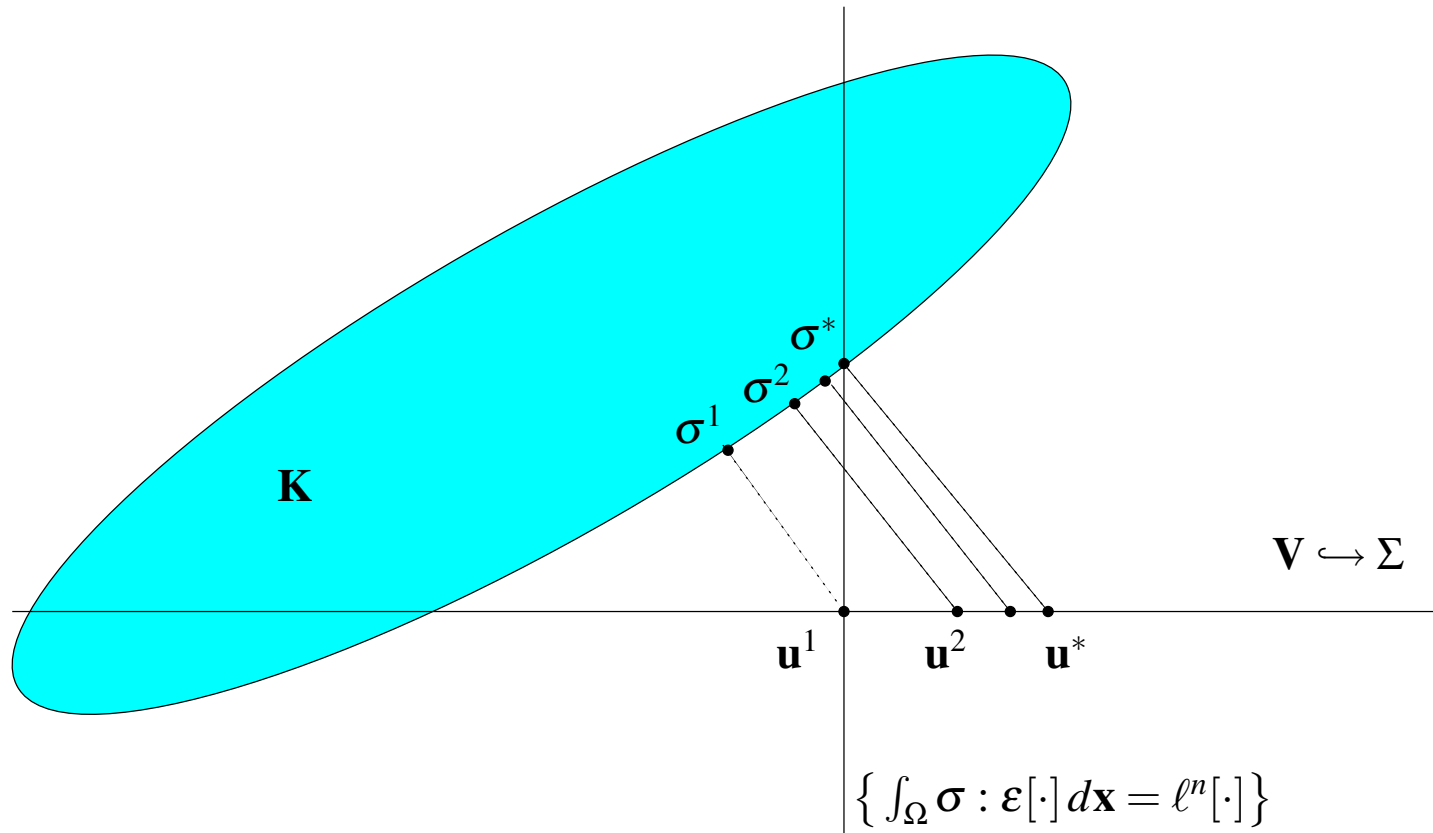
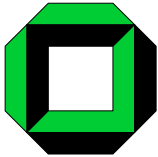


illustration of the projection method for $\varepsilon_p = \mathbf{0}$



II. The Lagrange-Newton method

Alternatively, one can consider the full system: find $(\sigma^n, \gamma^n, \mathbf{u}^n) \in \Sigma \times \Lambda \times \mathbf{V}(\mathbf{u}_D^n)$ with

$$\mathcal{F}^n(\sigma^n, \gamma^n, \mathbf{u}^n) = 0 ,$$

$$\text{where } \mathcal{F}^n(\sigma, \gamma, \mathbf{u}) = \begin{pmatrix} \sigma - \mathbf{C} : (\varepsilon(\mathbf{u}) - \varepsilon_p^{n-1}) - \gamma D\phi(\sigma) \\ \max\{0, \phi(\sigma)\} \\ \int_{\Omega} \sigma : \varepsilon[\cdot] d\mathbf{x} - \ell^n[\cdot] \end{pmatrix} .$$

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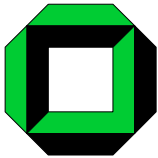
A semismooth Newton iteration

$$0 \in \mathcal{F}^n(\sigma^{n,k-1}, \gamma^{n,k-1}, \mathbf{u}^{n,k-1}) + \partial \mathcal{F}^n(\sigma^{n,k-1}, \gamma^{n,k-1}, \mathbf{u}^{n,k-1}) \begin{pmatrix} \Delta \sigma^{n,k} \\ \Delta \gamma^{n,k} \\ \Delta \mathbf{u}^{n,k} \end{pmatrix}$$

is well defined, although in general $\partial \mathcal{F}^n(\sigma^{n,k-1}, \gamma^{n,k-1}, \mathbf{u}^{n,k-1})$ is not regular.

The algorithmic realization has the same structure as the projection method with the same formula for the consistent linearization and a modified right-hand side.

The complementary conditions (Kuhn-Tucker) are not guaranteed!



III. The SQP method

Inserting the linearized complementary conditions in the Lagrange-Newton system yields the SQP method. Every Newton step is replaced by the KKT-system of a quadratic program:

$$(FR_{n,k}) \quad 0 = \sigma^{n,k-1} - \mathbf{C} : (\boldsymbol{\varepsilon}(\mathbf{u}^{n,k-1}) - \boldsymbol{\varepsilon}_p^{n-1}) - \gamma^{n,k-1} D\phi(\sigma^{n,k-1}) \\ + \Delta\sigma^{n,k} - \mathbf{C} : \boldsymbol{\varepsilon}(\Delta\mathbf{u}^{n,k}) - \Delta\gamma^{n,k} D\phi(\sigma^{n,k-1}) - \gamma^{n,k-1} D^2\phi(\sigma^{n,k-1}) \Delta\sigma^{n,k},$$

$$(KT_{n,k}) \quad \phi^{n,k}(\sigma^{n,k}) \leq 0, \quad \gamma^{n,k} \phi^{n,k}(\sigma^{n,k}) = 0, \quad \gamma^{n,k} \geq 0,$$

$$(EE_{n,k}) \quad \int_{\Omega} \sigma^{n,k} : \boldsymbol{\varepsilon}(\mathbf{v}) d\mathbf{x} = \ell^n[\mathbf{v}],$$

where $\phi^{n,k}(\sigma) = \phi(\sigma^{n,k-1}) + D\phi(\sigma^{n,k-1}) : (\sigma - \sigma^{n,k-1})$ is the linearized flow function.

The SQP-step is equivalent to the following nonlinear variational problem: for given $\boldsymbol{\varepsilon}_p^{n-1}$ and $\sigma^{n,k-1}$, $\gamma^{n,k-1}$ find $\mathbf{u}^{n,k} \in \mathbf{V}(\mathbf{u}_D^n)$ such that

$$\int_{\Omega} P^{n,k}(\mathbf{C}^{n,k} : (\boldsymbol{\varepsilon}(\mathbf{u}^{n,k}) - \boldsymbol{\varepsilon}_p^{n-1})) : \boldsymbol{\varepsilon}(\mathbf{v}) d\mathbf{x} = \ell^n[\mathbf{v}], \quad \mathbf{v} \in \mathbf{V}(\mathbf{0}),$$

where $\mathbf{C}^{n,k} = (\text{id} + \gamma^{n,k-1} D^2\phi(\sigma^{n,k-1}))^{-1} : \mathbf{C}$. The semismooth Newton iteration reads

$$0 \in F^{n,k}(\mathbf{u}^{n,k,m-1}) + \partial F^{n,k}(\mathbf{u}^{n,k,m-1}) \Delta\mathbf{u}^{n,k,m}, \quad \mathbf{u}^{n,k,m} = \mathbf{u}^{n,k,m-1} + s^{n,k,m} \Delta\mathbf{u}^{n,k,m}, \quad m = 1, 2, 3, \dots$$

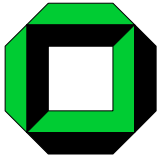
where $F^{n,k}(\mathbf{u})[\mathbf{v}] = \int_{\Omega} P^{n,k}(\mathbf{C}^{n,k} : (\boldsymbol{\varepsilon}(\mathbf{u}) - \boldsymbol{\varepsilon}_p^{n-1})) : \boldsymbol{\varepsilon}(\mathbf{v}) d\mathbf{x} - \ell^n[\mathbf{v}]$ and $s^{n,k,m} \in (0, 1]$.

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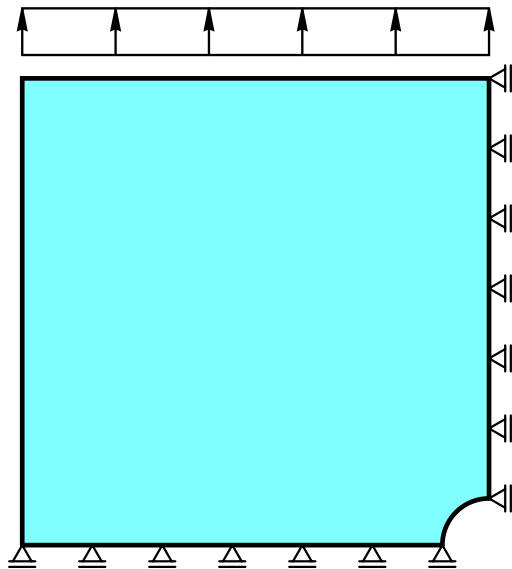
A 2-d benchmark revisited

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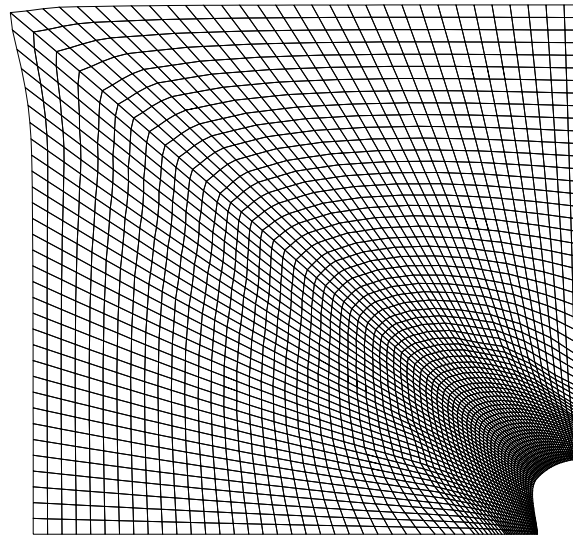
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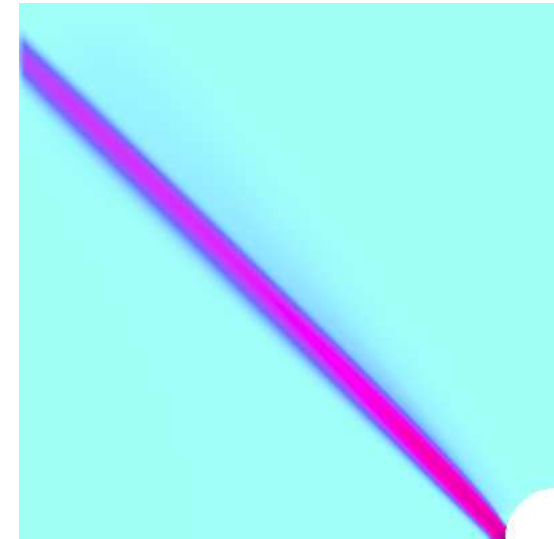
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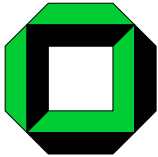
geometry and boundary conditions



deformation for $t = 4.7$



equivalent plastic strain



A 2-d benchmark revisited

Projection method			SQP method			inexact SQP method		
(FR)	(KT)	(EE)	(FR)	(KT)	(EE)	(FR)	(KT)	(EE)
ϵ	ϵ	24.76562	115.12502	5.093109	ϵ	114.98518	5.089170	0.8500337
ϵ	ϵ	17.87826	43.03050	0.797243	ϵ	43.02612	0.825375	0.0441101
ϵ	ϵ	13.17991	0.78454	0.074983	ϵ	0.78377	0.074904	0.1351428
ϵ	ϵ	9.66825	0.00294	0.000073	ϵ	0.00291	0.000150	ϵ
ϵ	ϵ	6.38058	ϵ	ϵ	ϵ	ϵ	ϵ	ϵ
ϵ	ϵ	4.38372						
ϵ	ϵ	3.32549						
ϵ	ϵ	0.66842						
ϵ	ϵ	0.00188						
ϵ	ϵ	ϵ						

$t = 4.6, \Delta t = 0.3$

reduction to a defect $\epsilon < 10^{-10}$

16384 cells

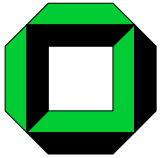
cells	dof	Projection method	SQP method	inexact SQP method
4096	8450	9 Newton steps	5 SQP steps (18 substeps)	5 SQP steps (10 sub.)
16384	33282	10 Newton steps	5 SQP steps (21 substeps)	5 SQP steps (14 sub.)
65536	132098	17 Newton steps	5 SQP steps (23 substeps)	5 SQP steps (16 sub.)
262144	526338	31 Newton steps	5 SQP steps (31 substeps)	5 SQP steps (22 sub.)
1048576	2101250	56 Newton steps	5 SQP steps (42 substeps)	5 SQP steps (31 sub.)

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A 3-d example

25600 hexahedra

87363 unknowns

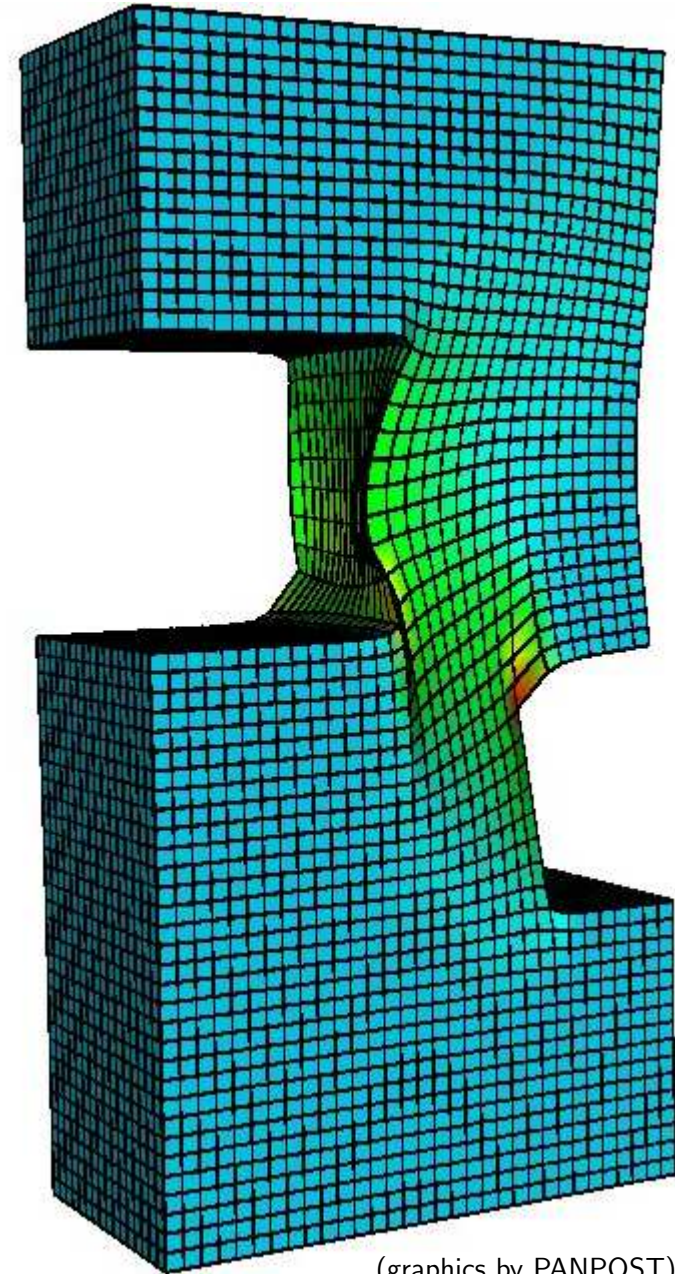
100 loading steps

310 inexact SQP steps

350 Newton steps

12 processors

2 h 10 min computing time



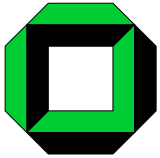
(graphics by PANPOST)

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Conclusion

- Convex programming gives a better understanding of computational plasticity.
- The numerical experiment reflects the fact that the primal displacement approximation in H^1 is not well-posed, but the dual stress approximation in L_2 is well-posed.
- The classical **Projection Method** is efficient for small loading steps.
- The SQP method can be realized as a **Linearized Projection Method** with only small algorithmic modifications.
- Close to the limit load the SQP method has better global convergence.
- The SQP method can be generalized to a broad class of mechanical problems with unilateral constraints.

